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TRANSONIC FAN/COMPRESSOR ROTOR DESIGN STUDY

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Volume II

D.E. Parker and M.R. Simonson
General Electric Company
Aircraft Engine Business Group
Advanced Technology Programs Dept.
Cincinnati, Ohio 45215

February 1982

Final Report for Period September 1980 - February 1982

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This technical report has been reviewed and is approved for publication.

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the five designs deviate from		
		tric variations are specified
at the rotor tip. The origin	nal hub characteris	stics were preserved to the
maximum extent practical. The		

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This volume describes the aerodynamic design details of the Phase I Rotor. The Phase I rotor has the tip airfoil maximum thickness located at 40% of meanline length as compared with 70% for the baseline rotor. The location of maximum thickness varied line rly with radius to 56% of meanline length at the hub, which is the same as the baseline rotor.

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VOLUME II

PHASE I ROTOR DESIGN

FOREWORD

This Final Technical Report was prepared by the Advanced Technology Programs Department, Aircraft Engine Business Group, General Electric Company, Evendale, Ohio for the United States Air Force Systems Command, Air Force Wright Aeronautical Laboratories Wright-Patterson Air Force Base, Ohio under Contract F33615-80-C-2059. The work was performed over a period of one year starting in September 1980. Effren Strain (Captain USAF) was the Air Force Project Engineer for this program.

This report describes the results of an effort to aerodynamically define five rotor designs, all parametrically related to a base line design which could be evaluated by future testing in order to define the sensitivity of transonic blade rows to several design variables.

For the General Electric Company Mr. D.E. Parker was the Technical Program Manager for this program. Mr. M.R. Simonson was the principal investigator. Mr. A.J. Bilhardt was the overall Program Manager.



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LIST OF SYMBOLS AND ABBREVIATIONS

1. Used in Circumferential Average Flow Output Tables

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RATIO

STA	calculation station number	
WIF	total airflow	
PSIC	stream function (0 = tip (OD), 1 = hub (ID))	
2	axial location-	inches
R	radius	inches
PHI	streamline slope	degrees
CURV	streamline curvature — = neg., — pos.	1/inches
VM	meridional velocity	ft/sec
cu	absolute tangential velocity	ft/sec
ALPHAM	absolute flow angle on stream surface	degrees
M	meridional Mach number	•
SL	calculation streamline number	
BLDBLK	flow blockage factor free area - 1	blocked area/free area
PS	static pressure	psia
PT	total pressure	psia
TT	total temperature	degrees
BETAM	relative flow angle on stream surface	degrees
UREL	relative velocity	ft/sec
MREL	relative Mach number	
VABS	absolute velocity	ft/sec
MABS	absolute Mach number	
GAMMA	specific heat ratio	
PT-RAT	total pressure/inlet total pressure	
TT-RAT	total temperature/inlet total temperature	
RCU	radius x tangential velocity	in-ft/sec
CZ	axial velocity	ft/sec
PCT IMM	percent annulus immersion from tip (OD)	
RAD	average of leading and trailing edge	inches
ACC PT		
RATIO	cumulative total pressure ratio	
ACC TT	which the same and the same and the	

cimulative total temperature ratio

LĪST OF SYMBOLS AND ABBREVIATIONS

1. Used in	Circumferential Average Flow Output Tables (Cont'd)	
AD.	adiabatic efficiency	
POLY	polytropic efficiency	
Axial VEL R	axial velocity ratio across blade row	
2. Used in	Stream Surface Blade Coordinate Tables	
PT	point number	
PCT X	fraction of meridional distance from leading edge	
x	meridional coordinate on meanline	inches
Y	tangential coordinate on meanline	inches
B*M	meanline angle on stream surface	degrees
T(M)	thickness of blade perpendicular to meanline	inches
XS	meridional coordinate on suction surface	inches
YS	tangential coordinate on suction surface	inches
XP	meridional coordinate on pressure surface	inches
YP	tangential coordinate on pressure surface	inches
3. <u>Used in</u>	Plane Section Coordinate Tables	
2	axial coordinate of stacking axis	inches
R	radius of coordinate system origin	inches
MU	tilt angle in axial direction	degrees
ETA	tilt angle in tangential direction	degrees
RHO	section height	inches
PT	point number	
ALPHA	axial coordinate	inches
ZETA*	meanline angle from axial	degrees
UPSILON	coordinate perpendicular to ALPHA and radius	inches
PCT AL	fraction of axial distance from leading edge	

local thickness/chord ratio

T/C

SECTION V11

DESIGN OF PHASE I ROTOR

1. INTRODUCTION

The specification of the chordwise location of airfoil maximum thickness of the transonic/compressor rotors has often been defined more on the basis of historical practice than on a knowledge of its aerodynamic effect. Research by NASA in the 1950's generally indicated that as relative inlet Mach numbers rose, it was desirable to move the location of maximum thickness aft on an airfoil.

The early work, however, was done with airfoils having significant positive camber. Today, many airfoils have little overall relative turning in the tip region, and frequently have S-shaped meanlines: negative camber followed by some positive camber. In some cases, a forward shift in maximum airfoil thickness may help achieve the desired airfoil suction surface shape, with a less S-shaped meanline. There is also incentive to move the maximum thickness forward to make the blade more capable of withstanding a bird strike without excessive damage.

To get more definitive aerodynamic data on the effect of the location of airfoil maximum thickness, the Phase I blade has been designed with the maximum thickness located at 40% and the Phase II blade with maximum thickness at 55%, compared with the baseline rotor which has its tip maximum thickness at 70% of meanline length.

2. DESIGN PROCEDURE

The "data match" circumferential average flow solution, which was previously described in Vol. I, was used as a starting point for the design of the Phase I rotor. The annulus blockage used in the internal blade calculation stations was adjusted to be consistent with the forward shift of the airfoil maximum thickness. The assumed chordwise distribution of work was iteratively adjusted to obtain a calculated chordwise distribution of static pressure similar to that of the data match calculations of the baseline rotor. Also the blade meanline departure angles (the difference between the air angle and the meanline angle) were adjusted to maintain the same throat

area and flow induction capacity as the baseline blade. To adjust for the increased blade blockage in the forward half of the blade, and to better match the data match static pressure distribution in the hub, the hub contour internally within the rotor was modified slightly relative to the baseline rotor. The two hub contours are compared in Figure 19.

After each modification to the chordwise work distribution and/or departure angles, revised blade annulus blockage and blade lean angles were calculated and input to the circumferential Average Flow Determination (CAFD) computer program for the next iteration.

The rotor exit radial distribution of total pressure and temperature was maintained the same as the data match of the baseline rotor.

THE PARTY OF THE P

The resulting streamline static pressure distribution for the Phase I blade is compared with the data match of the baseline rotor on Figure 20.

The assumed streamline work input (as a fraction of the total streamline work) is plotted versus percent axial projection in Figure 21. The tip streamline is the one on the left. Each subsequent streamline is indexed to the right by the value of its stream function (fraction of the total flow from the tip). The dashed lines are lines of constant percent axial projection.

A method of characteristics computer program was used to analyze the flow in the cascade flow induction region for streamlines 3 and 6 to assure that the rotor would achieve the design flow. For other streamlines, the difference between the suction surface angle and the "free flow" streamline angle was compared with similar data from the data match calculations of the baseline rotor. This then, was used as a guide in setting the suction surface angle in the flow induction region.

To satisfy the same flow induction capacity as the baseline blade, it was required to use larger meanline incidence angles as a result of the larger blade leading edge wedge angle resulting from the forward location of maximum thickness. Phase I blade incidence angles are shown on Figure 22.

A modified version of Carter's Rule was used to calculate a reference deviation angle for the baseline rotor. This procedure converts the vector diagrams (from the data match calculations) to an equivalent two-dimensional

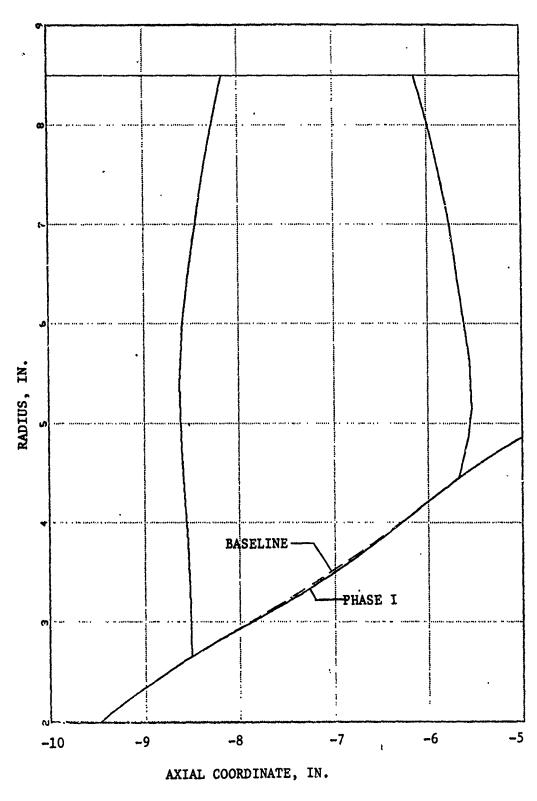


Figure 19. Comparison of Phase I Rotor Hub Contour to Baseline Rotor Hub Contour

set of vectors which would produce the same circulation as the actual blade taking into account the change in streamline radius and meridional velocity. The difference between the deviation angle implied by the data match calculations and the reference deviation angle was then added to the reference deviation angle calculated from the modified Carter's Rule for the Phase I blade. Phase I Rotor deviation angles are shown on Figure 23. A plot of departure angles for each streamsurface section is shown in Figure 24. Once the intrablade work distribution was chosen these departure angles were required to satisfy the desired incidence angles, deviation angles, and passage area ratios. The resulting streamsurface tip section of the Phase I rotor is compared to that of the baseline rotor in Figure 25. The "deviation angle minus reference deviation angle" for the Phase I rotor was kept essentially the same as the data match analysis although there are some small differences. Figure 26 shows the "delta deviation" compared to the data match of the baseline design.

If the performance of a new rotor design is to be accurately evaluated by comparing overall stage performance with the baseline design then it is important that the stator have nearly the same entering conditions in both cases. Figure 27 shows a comparison of the Phase I stator incidence angles with the data match base. As can be seen the differences are small.

Figure 28 shows the radial distribution of Phase I rotor throat margin and compares it to the data match case. The throat margin for a streamsurface blade section is defined here as the percent of excess throat area over and above the minimum theoretical area required to pass the streamtube flow at a throat Mach number of 1.0 and assuming a total pressure loss equivalent to a normal shock at the upstream Mach number. In a rotor the effect of radius change (between the leading edge and throat) on the relative total enthalpy and pressure is included. As can be seen in Figure 27 the Phase I rotor throat margin is nearly identical to that of the data match of the baseline design.

Details of the Phase I rotor design are given in Section VIII.

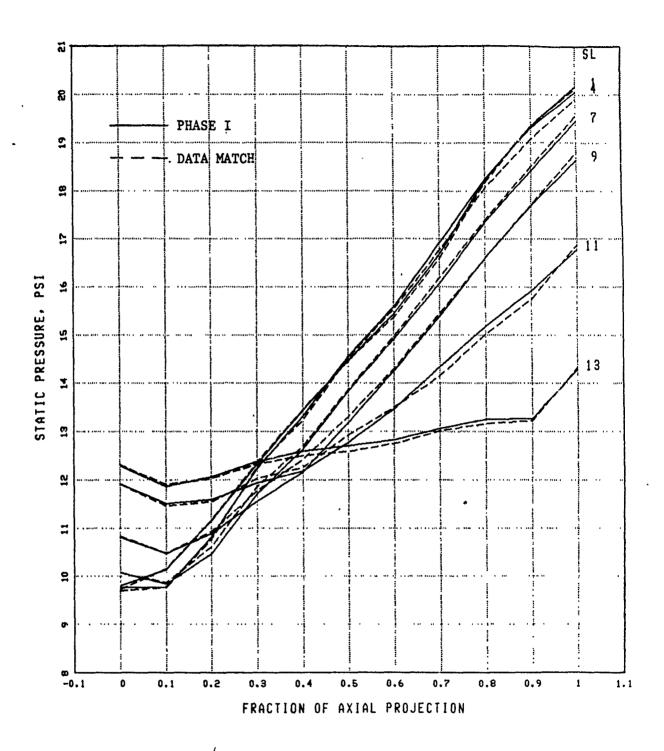
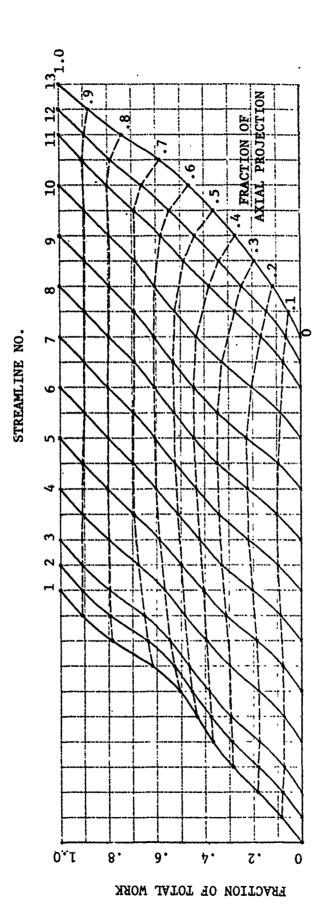


Figure 20. Phase I Rotor Static Pressure Distribution



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Figure 21. Phase I Rotor Intrablade Work Distribution

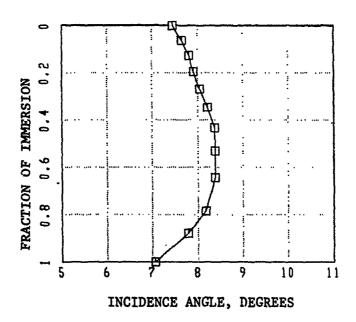


Figure 22. Phase I Rotor Incidence Angle Versus Fractional Immersion

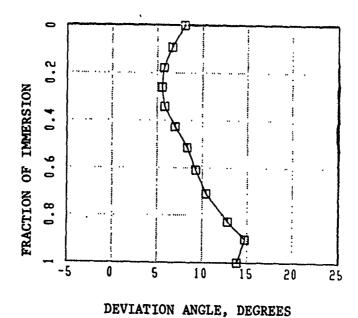
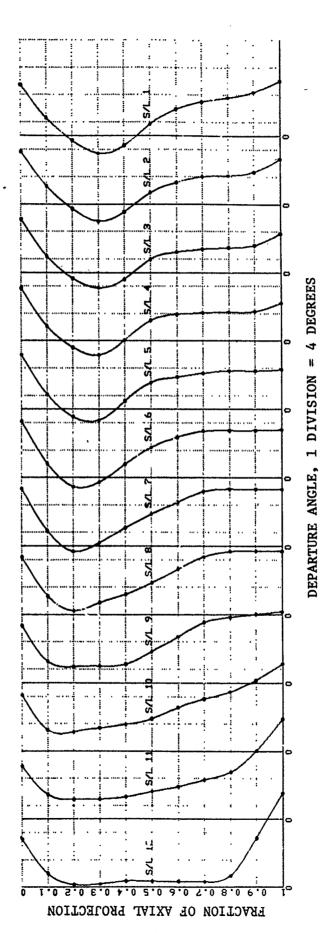


Figure 23. Phase I Rotor Deviation Angle Versus Fractional Immersion



Phase I Rotor Intrablade Departure Angle Distribution Figure 24

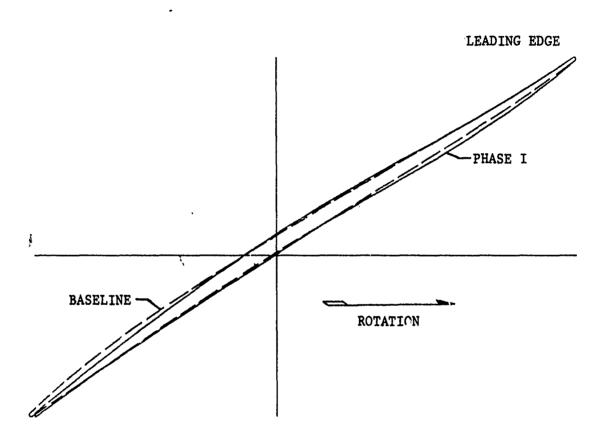


Figure 25 Phase I Rotor Streamsurface Tip Section Compared With Baseline Design

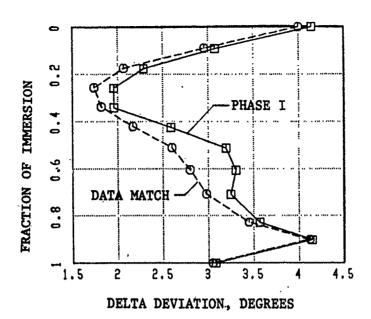
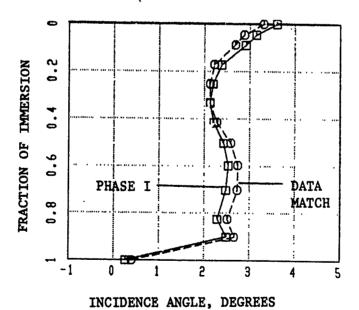


Figure 26 Phase I Rotor Deviation Angle Minus Reference Deviation Angle Compared With Data Match



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Figure 27 Phase I Stator Incidence Angle Compared With Data Match

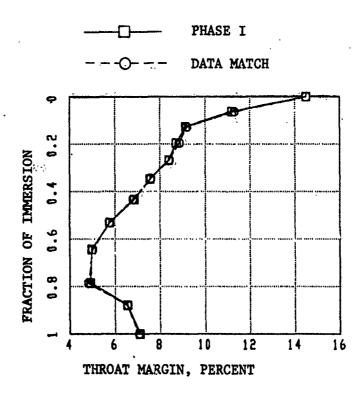


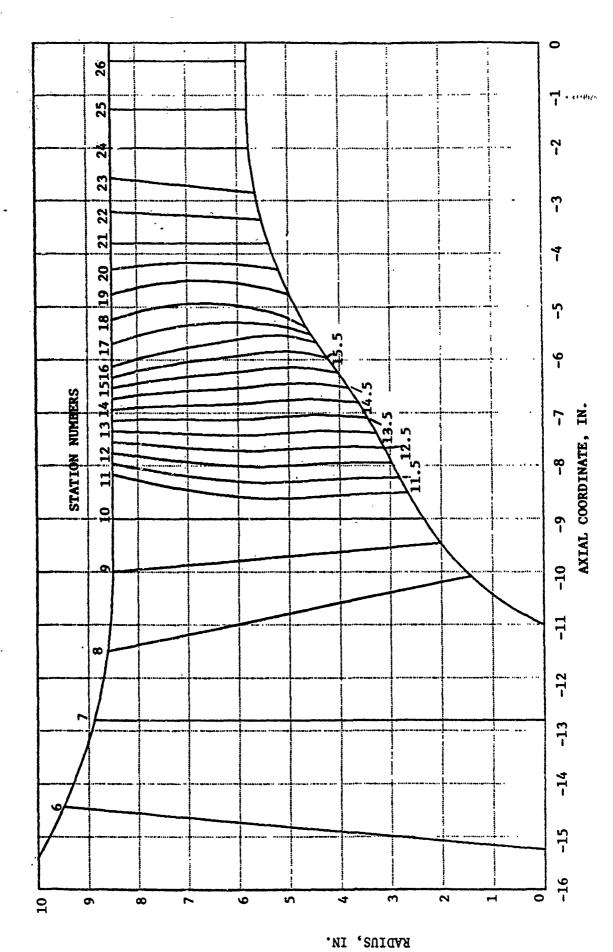
Figure 28. Phase I Rotor Throat Margin Compared With Data Match

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SECTION VIII DETAILS OF PHASE I ROTOR DESIGN

1. CIRCUMFERENTIAL AVERAGE FLOW SOLUTION

The following tabulation presents the detail results of the Phase I Rotor circumferential average flow computation. Each page of the tabulation gives results for one calculation station. Figure 29 shows the calculation station locations within the gas flowpath. At each calculation station various aero-dynamic parameters are given on each of thirteen calculation streamlines. Also given are several mass averaged station flow properties. The Phase I rotor blade forces are included at the end of this tabulation.



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Figure 29. Compressor Flowpaty With Calcuiation Stations

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STA 5.000 MASS AVERAGED PROPERTIES

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RCU= 0. VM= 255.3 CZ= 233.4 MM=0.230 MABS=0.230 WREL=1.300

MABS 0.395 0.474 0.464 0.464 0.464 0.466 0.466 0.471 0.495 0.395 0.395 0.395 0.369 0.471 0.471 0.471 0.471 0.471 0.471 0.476 0	0.361
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STA 6.000 MASS AVERAGED PROPERTIES

PT= 14.696 TT= 518.69 GAMMA=1.4016 PT-RAT= 1.000

RCU= 0. VM= 455.6 CZ= 438.5 MM=0.415 MABS=0.415 MREL=1.120

	D+H=0.	ABH=0.	Ī	0.578	0.571	0.564	0.549	0.533	0.518	0.502	0.486	0.468	0.446	0.415	0.390	0.347	MABS	0.578	0.571	0.564	0.549	0.533	0.518	0.502	0.486	0.468	0.446	0.415	0.390	0.347	
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STA	MTIP=		PHI	880 -15									237 -1	64 4	206 3	000	ΡŢ	14.696	14.696	14.696	14.696	14.696	14.696	14.696	14.696	14.696	14.696	14.696	14.696	•	
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		61.365	2	-12.800	-12.800	- 12.8(- 12.800	- 12.800	- 12.800	-12.800	-12.800	-12.800	-12.800	-12.800	-12.800	-12.800	BLOBLK	0.998	1 866	1 866	1 866	•	•	•	•	_	-	-	_	_	
TALET		WTF= 6	PSIC	ö	0.050	0.100	0.200	0.300	0.400	0.500	0.600	0.700	0.800	0.900	0.950	1.000	SLB	•	0	8	•	0	9	0	0	_	10	_	12 0	-	

STA 7.000 MASS AVERAGED PROPERTIES
PT= 14.696 TT= 518.69 GAMMA=1.4017 PT-RAT= 1.000
RCU= 0. VM= 539.1 CZ= 532.1 MM=0.495 MABS=0.495 MREL=1.109

D+H=0.	A BH=0.	Ī	0.665	0.656	0.646	0.628	0.611	0.595	0.578	0.560	0.538	0.509	0.467	0.427	0.395	MABS	0.665			0.628			_	0.560			-	0.427	0.395	8
	٠.	ALPHAM	ö	o.	o.	o.	o,	ö	ö	o O	o.	ò	o.	o.	o.	VABS	711.9	703.1	693.7.	675.6	658.6	642.1	625.0	606.3	583.9	554.6	510.6	468.1	434.0	
	ABC=(ö	ó	o,	ó	o.	ö	o.	o o	o O	ö	o.	ó	o .	MREL	1.567	1.533	1.497	1.424	1.349	1.269	1, 184	1.091	0.987	0.866	0.710	0.601	0.456	
224.06	O INBR=0	¥>	711.9	703.1	693.7	675.6	658.6	642.1	625.0	606.3	583.9	554.6	510.6	468 1	434.0	VREL	1677.5	1642.5	1606.4	1531.7	1453.3	1370.0	1280.5	1182.5	1072.2	942.7	776.9	559.1	501.2	MASS AVERAGED PROPERTIES
AFLOW=	ITYPE=0	CURV	-0.0953	-0.0964	-0.0909	-0.0815	-0.0743	-0.0694	-0.0667	-0.0666	-0.0695	-0.0768	-0.0935	-0.1212	0. 1910	BETAM	64.89	64.66	64.42	63.83	63.05	62.05	60.78	59.15	57.00	53.96	48.91	44.75	30.05	VERAGED
MTIP= 40	OPTY=FREE	=		-7.49 -0		-5.59 -0	-4.25 -0			83	.37	69.	12. to -c		66.	F	518.7	518.7	518.7	518.7	518.7	518.7	518.7	518.7	518.7	518.7	518.7	518.7	518.7	MASS AVERA
MTIP		Hd							-	0	m	320 6	318 12	•	4	PT	14.696	14.696	14.696	14.696	14.696	14.696	14.696	14.696	14.696	14.696	14.696	14.696	14.696	8.000
1= 4	OPTX=DPP	œ	499 8.608	∞	21 8.211	7	7.	9	52 6.333		960.2 60	4	e	'n	-	PS	20		1.092	1.260	1.416	1.565	1.716	1.879	2.069	2.310	2.654	12.965	3.199	STA
	61.365	7	-11.49	-11.461	-11.42	-11.339	-11.250	-11, 155	-11.052	- 10.938	- 10.809	-10.656	-10.459	-10.323	- 10.086	BLDBLK			_	₩.	0.997 11	-	-	_	_	_	_	_	_	:
	WTF= 61	PSIC	o.	0.050	0.100	0.500	0.300	0.400	0.500	0.600	0.700	0.800	0.900	0.950	1.000	36 86		0	9 9	⊙	5	9	7	8				12 0.	13 0.	į

CONTRACTOR OF THE PROPERTY OF

																			_			_					_				
	Ö.	ö.	_	12	05	0.697	383	0.669	553	336	0.614	286	550	0.501	0.472	468	MABS	0.712	0.705	0.697	0.683	0.669	0.653	0.636	0.614	0.586	0.550	0.501	.472	.468	
ш	D+H=0.	AB!:=0	Ī	0.712	0.705	Ö	ö	0	0	Ö	ö	0	Ö	ö	0	0	_	o	o	o,	Ö		o		0				0	ö	
FREE	_		X														VABS	758.2	751.2	743.3	729.6	5.6	700.5	2.9	5.3	ე ა.	596.6	546.2	5.4	1.5	
			ALPHAM	ö	ö	o	ö	ö	o	ö	ö	o	o	ö	Ö	ö	>	75	75	7	72	715	2	682	661	633	S	3	515	S	
	D+C=0	ABC=0	•														Ę	79	80	5	80	78	303	223	33	32	912	762	667	269	
	۵		5	ó	o	o.	o.	o.	o.	o	ó	o O	ó	ö	o	ó	MREL	1.579	1.548	1.515	1.448	1.378	Ę.	4.2	1.133	1.032	9.9	0.7	9.0	0.5	
	9	INBR-0																7	ĸ,	0	ı,	က	'n	r.	6	~	۲.	-	۲.	ri.	
	211.86	Z	¥	8.2	1.2	3.3	9.6	5.6	0.5	5.9	£.	3.5	9.9	6.2	5.4	11.5	VREL	1680.7	1648.5	1615.0	546	474	397	313	220.	115.2	989.7	830	728.	622	
		Q a	¥	758	751	743	729	715.	9	682	661	633	296	546	5 15	5	_	Ī	-	•	_	_	_	_	_	_	_		_	S	
	AFLOW	ITYPE =0	>		=	23	3	ဗွ	56	88	ဓ္ထ	7	95	7,7	8	8 1	BETAN	63.19	2.8	62.60	1.8	60.96	9.91	58.68	57.20	55.39	52.93		4.99	4.7	
	AF		ರ		-0.054	-0.0523	-0.0504	-0.0506	-0.0526	-0.0568	-0.0630	-0.0714	-0.0795	-0.0812	-0.0406	. 18	80	Ú	9	9	9	Φ	59	Ñ	ເດ	ù	n	4	4	n	
000	2	REE		0	P	P	P	Ŷ	Ŷ	Ŷ	P	P	P	P	Ģ	0	•	7	7	2.4	7.	3.7	7.3	8.7	3.7	3.7	7.	7.	7.	3.7	
			—		Ξ	-0.89	-0.29	.58	. 73	3.25	20	•	1.18	9.	.63	. 65	H	5 18	5 18	5 18	518	518	518	5	-	518	518	5 18	518	518	
TAX	MTIP	9	PHI	0	1.1	Ŷ	Ŷ	ó	-	n	N,	7	Ξ	16	2	38		969	969	969	969	969.	969.	969.	969	969.	969	969	969	969	
•	? X			200	315	125	727	4	851	358	8 16	201	475	542	919		T	7	14.6	14.6	14.6	17.	14.6	14.6	14	14.6	12.6	14.6	7	4.	
	N.	OPTX=OPP	~	. S	60	8.1	•	7.304	6.8	•		•	•	3.5	2.9	2.0		Ç	, -	o o	-	ក	o.	<u>ლ</u>	2	~	_	~	7	<u></u>	
		OPT	•	6	4	80	ະຕ	2	22	-	776	725	5	37	536	460	8	473	541	10.619	0.751	3.885	1.029	1, 193	1.392	1.642	1.96.1	2.377			
		167	7	9.99		9.968	9.935	900	-9.862	3.821	7.	7.	-9.665	9.587		•	.	֝֞֝֝֝֝֝֟֝֝֟֝֝֟֝֝֟֝֝֟֝֟֝				•	-	÷	-	-	÷	-	-	*	
		365	,	۲.	ĭ	Ϋ.	Ĭ.	6-	7.	7	1	ĭ	7	ĭ	7	ĩ	A DRIK		966	966	966	966	966	966	966	966	966	966	966	966	
		9	PSTC	1	50	8	8	8	8	8	8	8	8	000	950	8	ă	ģ		Ġ	•			o			•	•			
TAINE	ב ה	ITE	ă	0	0	0	C	0	0	0	0	0	0.800	0	0	-	ī	7	٠ ،	i (?	4	· K	9	7	α	Ø	0	-	5	<u>t</u>	

STA 9.000 MASS AVERAGED PROPERTIES
PT= 14.696 TT= 518.69 GAMMA=1.4018 PT-RAT= 1.000 TT-RAT= 1.000
RCU= 0. VM= 663.8 CZ= 655.3 MM=0.617 MASS=0.617 MREL=1.178

E D•H=O.	ABH=0.	E	0.727	0.727	0.727	0.725	0.719	0.709	0.693	0.670	0.635	0.588	0.529	0.491	0.499	MABS	0.727	•	•	0.725	0.719	0.709	0.693	0.670	0.635	0.588	0.529	0.491	0.499	T= 1.000
A B	0	ALPHAM	ó	ó	o.	oʻ	o.	o O	Ö	o	ó	ó	o.	o.	o.	VABS	772.2	772.5	772.5	770.1	764.4	754.7	739.7	716.8	682.7	635.0	574.8	535.8	544.1	. ₹
D+C=0.	ABC		ö	ö	o O	ö	ö	ö	o.	ó	ó	ó	ó	ö	ö	MREL	1.588	1.562	1.534	1 476	1,413	1.345	1.269	1.182	1.080	0.957	0.854	0.707	0.627	9
204.14	O INBR=0	¥ >	772.2	772.5	772.5	770.1	764.4	754.7	739.7	716.8	682.7	635.0	574.8	535.8	544.1	VREL	1687.1	1658.6	1629.4	1568.3	1502.8	1431.8	1353.5	1264.8	1160.7	1034.2	874.3	770.9	683.0	MASS AVERAGED PROPERTIES MMA=1, 4018 PT-RAT= 1.00 7- E04 3 MM-0 EEC MARC
AFLOW*		CURV	٥.	0.0031	-0.0019	-0.0114	-0.0195	-0.0287	-0.0391	-0.0551	-0.0731	-0.0891	-0.0861	-0.0821	0.1922	BETAM	62.76	62.24	61.70	60.29	59.42	58.19	56.87	55.48	53.97	52.12	48.90	45.97	37.19	S AVERAGED
STA* 10.000 MTIP* 66	UPTY=FREE	HI			0.61	1.37 -(2.38 -(14.48 -(19.56 -(23.67 -(.46	Ħ	5 518.7	5 518.7	5 518.7	5 518.7	_	5 518.7	5 518.7	5 518.7	5 518.7	5 518.7	518.7	5 518.7		* C
	-0PP		8.500	8.317	8.130	7.742	7.332	6.895	5.423	5.905	5.319	1.626	3.733		340	pt	14.696	-	2	=	Ī	<u>.</u>	3 14.696	7	7	7	7	7	7	STA 10.000 TT= 518.69 (
1× 6		2	-9.000 -9.000		-9.000		. 000.6-		_		8		. 000.6-		800	X PS	5			_	·	10.507	10.653			7	12,145	12.460	12.	
INLET	WTF= 61.365	PSIC	· ·	0.050							-	·				St BLOBLK		2 0.994	3 0.994	4 0.994	5 0,994	6 0.994	7 0.994	_	9 0.994		0			PT= 14.696

~	D+H=0.	ABH=O.	Ī	0.783	0.784	0.785	0.787	0.784	0.774	0.754	0.721	0.677	0.624	0.555	0.512	0.511	MABS	0.783	0.784	. 0.785	0.787	0.784	0.774	0.754	0.721	0.677	0.624	0.555	0.512	7.11
LE ROTOR			LPHAM	ö		ó	o.	o o	ó	o.	°.	o.	o.	ö	o'	ö	VABS	825.2	826.4	827.3	828.8	826.5	817.0	8.767	766.2	723.3	671.1	601.7	557.9	120
	0*C=0.		7 33	o.	o.	ö	ó	o o	ó	ö	o.	o.	o	ó	ö	•	MREL	1.624	1.599	1.573	1.519	1.461	1.394	1.316	1.225	1.119	966.0	0.844	0.748	099 0
	197.55	INBR=3	X >	125.2	126.4	127.3	128.8	126.5	117.0	797.8	66.2	23.3	71.1	601.7	557.9	556.1	VREL	1712.0	1685.0	1657.4	1600.7	1539.5	1471.2	1393.3	1302.1	1195.9	1071.8	914.7	814.2	706 0
	AFLOW=	ITYPE=4		.0				_		-0.0292 7	_	-0.0564 7	-0.0663 6			0.1665 5	BETAM	61.18	60.63	90.09	58.82	57.53	56.27	55.07	53.95	52.78	51.23	48.87	46.75	Ç (7
11.000	: 79	OPTY *FREE		.0			44 0.	2			22	22	31	72 -0.	-0- 69	03 0.	F	518.7	518.7	518.7	518.7	518.7	518.7	518.7	518.7	518.7	518.7	518.7	518.7	1 0 1
STA	I						÷	0.7				*		21.	0 25.		F	4.696	4.696	14.696	4.696	4.696	4.696	4.696	14.696	4.696	4.696	4.696	4.696	202 7
	I= 7	OPTX=DPP	œ	6 8.500	80	&	7	7 7.360	9	1 6.473	2 5.966	Ŋ.		ю	•	4	PS	9.801	9.789	_	9.764 1	•	-		-		.302	11.918 1	.283 1	900
		. 365	2	-8.166	-8.20	-8.24	-8.32	-8.39	-8.46	-8.531	-8.59	-8.62	-8.60	-8.548	-8.526	-8.50	BLDBLK									0.990 10				
ROTOR 1		WTF= 61	PSIC	o.	0.050	0.100	0.200	0.300	0.400	0.500	0.600	0.700	0.800	0.900	0.950	4.000	Sr Bri	÷	2 0.9	9.0	₹	5 0.9	9	7	8	6.0	10 0.9	11 0.9	12 0.9	
ã		3																						:	20)				

STA 11.000 MASS AVERAGED PROPERTIES TT= 518.69 GAMMA=1.4018 PT-RAT= 1.000 TT-RAT= 1.000 VM= 754.0 CZ= 739.9 MM=0.710 MABS=0.710 MREL=1.259

PT= 14.696 RCU= 0.

28	D+H=0.	ABH=O.	I	0.805	0.811	0.817	0.839	0.854	0.860	0.850	0.822	0.785	0.734	0.663	0.623	909.0	MABS	0.806	0.812	,		0.855						0.666	0.626	0.609
IN ROTOR			ALPHAM	3.29	3. 10	2.82	2.80	2.93	3.34	3.96	4.39	4.68	4.87	5.47	5.59	5.99	VABS	856.9	861.6	866.6	886.3	8.006	6.906	899.7	874.1	838.7	788.9	718.1	677.7	660.0
	D*C=0.	3 ABC=0	2	49.2	46.6	42.6	43.3	46.1	52.8	62.2	66.7	68.4	6.99	68.4	0.99	68.9	MREL	1.584	1.566	1.549	1.511	1.466	1.408	1.335	1.248	1.151	1.038	0.891	0.805	0.723
	178.74	:5 INBR=3	X >	855.5	860.3	865.5	885.2	899.6	905.3	897.6	871.5	835.9	786.1	714.8	674.4	656.4	VREL	1684.3	1662.1	1640.8	1595.2	1543.9	1482.8	1408.8	1322.4	1225.1	1110.8	961.0	871.7	783.5
•	AFLOW*	ITYPE=5	CURY		0.0290	0.0311	0.0254	0.0150	-0.0010	-0.0058	0.0114	0.0205	0.0128	0.0299	0.0662	0.0917	BETAM	59.47	58.83	58.16	56.29	54.36	52.37	50.42	48.77	46.98	44.96	41.94	39.31	33.10
= 11.500		OPTY=PT	IHd	ö	13			2.59 (63	53	5			8.62 (Ħ	531.0	530.1	528.9								526.8		
STA=	MTIP=			500		141	765	372								815 2	PŢ	15.543	15.522	15.468	15.509	15.570	15.688	15.830	15.846	15.784	15.643	15.500	15.364	15.248
	I = 8	OPTX=T1	2	-7.963 8 .	89	_	7.	7.	_	Φ	-8.301 6.	S.	4	*	n		S	10.130	10,059	9.959	9.768	9.649	9.662	9.840	10.134	10.475	10.899	11.512	11.795	11.865
_		61.365	C				80	60	•							1	BLDBLK	0.944	0.944	0.943	0.940	0.935	0.927	0.917	0.907	0.898	0.886	0.865	0.847	0.812
ROTOR		WTF=	PSIC	ó	0.050	0.100	0.20	0.300	0.400	0.500	0.60	0.700	0.800		0 950	1.00	5	-	c	(P)	₹	Ŋ	ø	7	80	σ	5	-	5	1 3

oranismente estas proprios ("experiences "multipleters") describination ("multipleters") describing, "multipleters") ("multipleters") ("multipleters") ("multipleters") ("multipleters")

STA 11.500 MASS AVERAGED PROPERTIES
PT= 15.623 TT= 528.92 GAMMA=1.4018 PT-RAT= 1.063 TT-RAT= 1.020
RCU= 347.5 VM= 841.2 CZ= 824.5 MM=0.792 MABS=0.794 MREL=1.275

20	D+H=0.	ABH=0.	Ī	0.767	0.774	0.781	0.807	0.834	0.858	0.870	0.860	0.832	0.787	0.720	0.675	0.632	MABS	0.773	0.780	`	0.813				0.871	0.840	0.801	0.734	0.689	0.647
IN ROTOR			ALPHAM	7.30	7.18	6.92	6.88	7.12	7.73	8.51	9.17	10.28	10.78	11.09	11.53	12.33	VABS	837.0	842.9	848.7	873.1	899.2	923.7	937.9	929.2	905.9	861.0	792.5	747.0	703.0
	D+C=0.		3	106.3	105.3	102.3	104.5	111.4	124.2	138.8	148.0	161.6	161.0	152.4	149.3	150.2	MREL	1.499	1.480	1.464	1.430	1.392	1.346	1.290	1.219	1.127	1.026	0.898	0.814	0.719
	166.91	5 INBR=3	¥>	830.2	836.3	842.5	866.8	892.3	915.3	927.6	917.4	891.4	845.8	7.7.7	731.9	88.98	VREL	1622.2	1599.4	1578.2	1534.8	1488.5	1436.1	1375.1	1300.3	1207.2	1102.4	6.696	882.7	781.6
	AFI OW=	ITYPE=5	CURV	ö	0.0239	0.0342	0.0280	0.0222	0.000.0	0.0121	0.0007	0.0026	0.0309	0.0252	0.0116	0.0178	BETAM	59.22	58.47	57.73	55.61	53.17	50.40	47.58	45.13	42.41	39.89	36.69	33.98	28.52
STA= 12,000	MTTP=105	OPTY=PT	PHI	0.	1 9					6.66 C				.58	.84	7.61	11	545.3	544.5	543.2	542.6	542.9	544.2	545.4	545.1	545.0	542.0	537.3	534.7	
STA	118			8.500			07.77	_								965 27	ΡŢ	16,562	16.605	16.592	16.707	16.869	17.111	17.323	17.354	17.391	17.095	16.588	16.302	15.985
	5	OPTX=TT	7	759 8.		798 8.	٠	Ť		_	_					તં	8	11.147	11, 103	11.018	10.810	10.614	10.487	10.458	10.579	10.882	11.197	11.592	11.860	12.059
		61.365		-7.	-7.	-7.	-7.	-7	-7.					-7		-7.	2 K	913	0.912	0.911	0.907	839	.886	0.469	853	840	824	795	774	
POTOD 4		WTF= 6		C	0.050	0 100	0.200	0.300	0.400	0.500	0.600	0.700	0.800	0.900	0.950	80	, a	, -	. 0	0	4		9		8	_	_	, 0	12.0	-
		_																												

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STA 12.000 MASS AVERAGED PROPERTIES PT= 16.930 TT= 542.65 GAMMA=1.4018 PT-RAT= 1.152 TT-RAT= 1.046 RCU= 813.7 VM= 863.5 CZ= 846.4 MM=0.805 MABS=0.815 MREL=1.230

~	D+H=0.	ABH=O.	Ŧ	0.720	0.727	0.736	0.756	0.783	0.811	0.832	0.844	0.841	0.815	0.751	0.708	0.644	MABS	0.735	0.743	0.753	0.773	0.802	0.832	0.856	0.870	0.870	0.848	0.784	0.744	0.680
N ROT		•	ALPHAM	11.84	11.90	11.99	11.97	12.37	12.90	13.38	14.10	15.05	16.03	16.81	17.88	18.63	VABS	810.7	818.3	827.6	847.3	875.6	905.2	927.6	940.6	940.4	917.0	851.0	808.7	741.3
,	_	E3 ABC=0	2	166.3	168.7	172.0	175.8	187.6	202.1	214.6	229.2	244.2	253.2	246.2	248.2	236.8	MREL	1.407	1.386	1.365	-	~	-	1.205	•	1.086	1.002	0.884	0.805	0.705
	Ť.	:5 INBR=3	¥>	793.5	800.7	809.6	828.8	855.3	882.3	902.4	912.2	908.1	881.3	814.6	769.7	702.4	VREL	1551.9	1526.6	1501.5	1455.0	1406.8	1358.0	1306.5	1245.9	1173.4	1083.5	959.2	876.1	768.9
_	AFLOW=	ITYPE=5	CURV	o.	-0.0021	0.0074	0.0194	0.0145	0.0304	0.0244	0.0150	0.0202	0.0243	0.0112	-0.0116	.0568	BETAM	59.25	58.37	57.37	55.27	52.56	49.48	46.32	42.93	39.29	35.57	31.87	28.53	24.00
= 12.500	MTIP=118	PTY=PT	PHI		•	-0.30					9.06	. 13	68.	1.24	24.84 -(7.97 -0	11	560.3	560		_	559.5	560.3	560.2	559.9			_	546.3	540.4
			2	200		_		392			108	_	_	265 2		114 2	Fq	17.672	17.821	17.968	18.175	18.477	18.767	18.912	18.983	18.949	18.662	17.930	17.541	16.873
	1*10	UPTX.	2	.556 8.	.565 8.	.576 8.	.605 7.	-7.635 7.	.663 6.	691 6.	.719 6.	724 5.	.690 5.	.645 4.	641 3.	.657 3.	PS	12.334	12.348	12.338	12.235	12.093	11.916	11.717	11.588	11.558	11.653	11.940	12.147	12.381
-		61.365	ည	-7.		.7-						-7	-	-7	-		BLDBLK	0.889	0.889	0.889	0.884	0.874	0.860	0.841	0.823	0.806	0.785		0.728	0.682
ROTOR 1		WTF=	PSIC	o.	0.0	0.100	0.2	٥. ک	0.4	0.50	0.600	0.70	0.800	0.90	0.9	÷.	SL	-	8	က	4	ប	9	7	æ	6	ō	=	12	ნ

THE TOTAL PROPERTY OF THE PROP

STA 12.500 MASS AVERAGED PROPERTIES
PT= 18.411 TT= 557.42 GAMMA=1.4017 PT-RAT= 1.253 TT-RAT= 1.075
RCU= 1315.6 VM= 854.8 CZ= 837.7 MM=0.786 MABS=0.810 MREL=1.162

80	D+H=0.	ABH=O.	Ŧ	0.669	0.682	0.694	0.723	0.753	0.785	0.810	0.830	0.840	0.830	0.780	0.740	0.661	MARC	9890		0.723									0.800	
IN ROTOR	ė.	ö.	ALPHAM	15.95	16.05	16.08	16.12	16.22	16.52	17.06	17.81	18.72	20.08	21.32	22.31	23.87	VARC	779.8	703 7	806.7	836.0	867.9	901.4	928.5	951.7	965.5	960.4	910.9	871.2	791.1
	D*C=0.		ລ	214.3	219.4	223.4	232.1	242.5	256.4	272.4	291.1	309.9	329.7	331.1	330.7	320.1	MOR	1.329	906	1.290	1.255	1.221	1.188	1.148	1.104	1.052	0.981	0.879	0.810	0.702
	153.32		¥>	749.8	762.7	775.1	803.2	833.4	864.2	887.7	906.1	914.4	902.0	848.6	806.0	723.5	VRF	1488.3	1463 3	1439.4	1394.3	1351.1	1307.5	1258.8	1205.3	1144.7	1066.4	956.8	882.9	7.797
0	AFLOW=	ITYPE=5	CURV	٠.	0.0199	0.0192	0.0228	0.0292	0.0221	0.0125	0.0206	0.0161	0.0070	-0.0109	-0.0332	0.1324	BETAM	59.75	20.00	57.42	54.83	51.92	48.63	45.15	41.26	36.98	32.24	27.52	24.08	19.54
A= 13.000	MTIP=131	OPTY=PT	PHI				0.23 (6.07	8.76	_	15.61	21.24 -0	25.26 -(29.72 -0	11	_			5 571.8								556.8	549.5
										.601	. 154	. 658	. 092	4.382	. 915	. 269	Ā	18.591		19.025		19.702								17.850
	I=11		Z	w	w	w	-7.366 7	•		•	-7.428 6	ស			.346 3	.374 3	PS	13.445	13.454	13.433	13.323	13, 118	12.867	12.632	12.384	12, 165	12.090	12.183	12.280	12.596
-		61.365	SIC											ì	950 -7	ر- د-	BLOBLK	0.879	0.879	0.879	0.874	0.866	0.852	0.831	0.810	⊘.788	0.763	0.729	0.702	0.653
ROTOR 1		WTF	ă.	ö	ö	0	0.200	0	ö	ö	• •	0	٠. ص	0.900	0.950	1.000	SL	•	8	က	4	S	ဖ	_	ထ	တ	9	=	5	+

STA 13.000 MASS AVERAGED PROPERTIES
PT= 19.656 TT= 569.16 GAMMA=1.4016 PT-RAT= 1.337 TT-RAT= 1.097
RCU= 1714.7 VM= 848.1 CZ= 830.6 MM=0.772 MABS=0.812 MREL=1.114

OR	D•H=0.	ABH=O.	Ī	0.617	0.635	0.648	0.677	0.708	0.739	r. 764	0.785	0.801	0.801	0.774	0.747	0.687	MABS	0.656	0.677									0.861	Ö	0.779
IN ROTOR	Ö.	O	ALPHAM	19.81	20.19	20.39	20.51	20.54	20.71	21.10	21.61	22.57	24.06	25.96	26.81	28.25	VABS	744 7	767.4	782.8	814.8	848.9	881.8	910.1	933.9	955.3	963.2	943.8	915.6	853.8
	D*C=0.	3 ABC=0	5	252.3	264.8	272.8	285.5	297.8	311.9	327.6	343.9	366.6	392.6	413.1	413.0	404.1	MREL	1.261	1.237	1.215	1.177	1.145	1.112	1.076	1.037	0.991	0.931	0.849	0.796	0.711
	150.88	5 INBR=3	Z >	700.6	720.3	733.8	763.1	794.9	824.8	849.1	868.2	882.1	879.5	848.6	817.2	752.1	VREL	1430.9	1402.2	1375.3	1327.7	1284.8	1242.0	1196.1	1147.2	1091.5	1022.2	930.2	871.5	779.0
_	AFLOW*	ITYPE=5	CURV		.0117	.0067	1.000.0	0.0194	.0127	.0230	.0177	.0094	.0102	.0313	-0.0519	-0.1167	BETAM	60.68	59.09	57.75	54.92	51.78	48.39	44.77	40.81	36.08	30.64	24.17	20.34	15.09
STA= 13.500	MTIP=144	TY=PT	IHd					1.38 0				11.59 0	15.64 -0		.05	2.15 -0	I	581.8	583.5	584.0	584.0	583.6	583.2	582.6	581.4	580.4	578.5	573.4	568.0	559.6
STA	_		<u>a</u>	200				7.407				720 1	177 15	500 2	57 26	39 33	PT	19.337	19.763	20.074	20.596	20.990	21.308	21.505	21.536	21.547	21.392	20.743	20.036	18.981
	I=12	OPTX*T1	CZ.	148 8.5	œ	_	•	127 7.4	•		_	5.	'n.	4	4	091 3.4	PS	4.480	4.538			14.361			3.504	3.188	2.956	2.776	12.664	12.701
		61.365	7	.7.	-7.1	-7.	-7.	-7.	-7.	-7.	-7.	-7.			-7.051	-7.0	LDBLK	0.883 1	.883 1		•								. 699	.648
ROTOR 1		WTF= 6	PSIC	ö	0.050	0. 100	0.500	0.300	0.400	0.500	0.600	0.700	0.800	0.900	0.950	1 .000	SL	-	0	0	4	2	9	4	0	6	0	110	12 0	13 0

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STA 13.500 MASS AVERAGED PROPERTIES PT* 20.889 TT* 580.28 GAMMA*1.4015 PT-RAT* 1.421 TT-RAT* 1.119 RCU* 2093.2 VM* 818.1 CZ= 799.9 MM*0.736 MABS*0.796 MREL*1.053

	0+H=0.	ABH=O.	Ŧ	0.576	0.595	0.610	642	919	706	726	744	757	762	754	742	708	MABS	0.630	0.653	0.671	90.706	0.743	0.777	.800	0.823	.845	.862	.871	0.868	.838
N ROT		•	_	_			.51	24.54 0.1		24.84 0.	25.36 0.	26.34 0.	27.91 0.	30.01 0.	31.23 0.	32.29 0.			749.3 0			843.6						961.9	955.9	919.7
		ABC=(CC CC	294.0	308.6	_		350.4	366.3	377.9		417.5	447.6	481.1	495.6	491.3	MREL	1.197	1.172	1.150	1.114	1.081	1.049	1.015	0.976	0.930	0.877	0.813	0.775	0.721
	149.38	=5 INBR=3	¥>	661.1	682.8	€99.4	732.7	767.4	97.6	816.4	832.1	843.2	845.2	833.0	817.4	777.5	VREL	1375.4	1345.1	1317.3	1270.4	•	1185.4	1140.9	-	_	972.5		853.7	791.5
٥	AFLOW=	ITYPE=5	CURV	Ġ.	-0.0162	-0.0058	-0.0014	-0.0085	0.0073	0.0125	0.0094	-0.0002	-0.0122	-0.0414	-0.0626	-0,0917	BETAM	61.27	59.49	57.93	54.78	51.30	47.71					21.87	16.77	10.80
STA= 14.000	MT1P=157	OPTY=PT	PHI	ö			•			50		•	15.84	30		34, 17 -	Ħ	4 592.2		_		6 595.1							_	
ST	_	TT	α	8.500	8.316	8. 135	7.774	7.413	7.045	6.658	6.240	5.781	5.263	4.621	4.204	3.624	T d	0 20.174			2	•				6 22.746		•		20.
	1=13		7	-6.945	-6.925	-6.909	-6.888	-6.873	-6.861	-6.852	-6.846	-6.824	-6.777	-6.742	-6.756	-6.808	LK PS	#:		_	_	•	_	4	14	7	E	13	5	4
ROTOR 1		WTF= 61.365		0.		0.100		0.300		200		0.700	8	_		4.000	St. BLDBLK		2 0.888	3 0.887	4 0.883	5 0.876	6 0 864	7 0.846	8 0.827	9 0.805	10 0.780	11 0.744	12 0.71	13 0.662
RC		5																						2	26					

STA 14.000 MASS AVERAGED PROPERTIES PT= 22.107 TT= 590.86 GAMMA=1.4014 PT-RAT= 1.504 TT-RAT= 1.139 RCU= 2453.2 VM= 789.4 CZ= 770.6 MM=0.703 MABS=0.784 MREL=0.997

υκ D∗H=O.	ABH=O.	¥	0.534	0.551	0.565	0.601	0.638	0.668	0.687	0.699	0.710	0.715	0.725	0.726	0.721	MABS	0.617	0.638	0.654	0.693	0.733	0.763	0.784	0.802	0.823	0.842	0.881	0.894	0.897	(T= 1,163
x x0		ALPHAM	30.10	30.17	30.16	29.88	29.44	28.97	28.93	29.34	30.34	31.88	34.60	35.75	36.58	VABS	719.6	742.8	759.7	801.6	843.0	872.1	891.7	907.0	927.3	944.6	981.4	991.8	987.7	2
D.C=0.	3 ABC=0	3	360.9	373.4	381.7	399.4	414.3	422.4	431.4	444.4	468.5	498.9	557.2	579.4	538.6	MREL	1.113	1.089	1.068	1.033	1.007	0.982	0.951	0.913	0.868	0.818	0.767	0.746	0.725	e (
148.88	5 INBR=3	¥	622.6	642.2	656.8	695.0	734.2	762.9	780.4	790.7	800.3	802.1	807.8	804.9	793.1	VREL	1298.2	1268.6	1241.5	1195.4	1157.5	1122.5	t0e1.1	1032.6	978.2	917.4	855.1	827.0	7.797	
AFLOW=	ITYPE=5	CURV		0.0044	-0.0106	-0.0155	-0.0054	0.0041	-0.0015	-0.0051	-0.0107	-0.0233	-0.0411	-0.0590	-0.0685	BETAM	61.34	59.59	58.06	54.45	50.63	47.18	43.79	40.03	35.11	29.03	19.15	13.27	6.19	MASS AVERAGED PROPER GAMMA=1.4012 PT-RAT=
STA= 14.500 MTIP=170	TP=YTQD		о	-0.24 0	i						11.60 -0	. 17	80	30	.75	1	608.9	610.0	610.0	610.0	609.1	606.4	603.5	8009	599.2	597.2	596.5	593.0	584.9	MASS AVE
STA=			9				_	(7)			•	16	23	28	35	Ą	21.561	22.100	22.510	23.315	23.888	24.113	24.138	24.039	24.018	23.867	23.760	23.210	22.032	8,
1=14	DPTX=TT	α	41 8.500		_	•	18 7.419	•			-		41 4.747	Y	10	Sd	16.676					_			•			-	3.058	STA 14, 50 TT= 603, 10
	61,365	2	-6.741	-6.712	-6.687	-6.648	-6.618	-6.593	-6.572	-6.554	-6.523	-6.472	-6.44	-6.46	-6.5	i i i			•	•	•			Ī	•	•	•	•	*	PT= 23.556
ROTOR 1	WTF= 6	S	0	0.050	0.100	0.500	0.300	0.400	0.500	0.600	0.700	0.800	0.900	0.950	.00	ĕ		8	0	4	8	9	7	8		10	Ī	120	0	P C
_	_	•																				_	_							

0R 0+H=0	ABH=0.	I	0.489	0.507	0.523	0.564	0.603	0.630	0.647	0.658	0.666	0.676	0.698	0.719	0.733	MABS	0.622	0.640	0.655	0.692	0.730	0.756	0.778	0.795	0.813	0.840	0.896	0.935	0.975	
N ROT		ALPHAM	38.21	37.64	36.97	35.45	34.30	33.62	33.66	34.10	34.98	36.50	38.82	39.78	41.25	VABS	738.9	758.5	773.5	811.7	849.5	874.3	894.1	909.3	926.2	952.3	1006.5	1042.6	1075.7	
I 0+0+0		20	457.1	463.2	465.2	470.8	478.7	484.1	495.6	509.8	531.0	566.4	631.0	667.1	709.3	MREL	1.005	0.987	0.974	0.954			0.882		0.803	0.760	0.727	0.728	0.733	
148 57	5 INBR=3	¥>	580.6	600.6	618.0	661.2	701.7	728.0	744.2	753.0	758.8	765.5	784.2	801.2	808.7	VREL	1193.6	1170.0	1150.0	1117.8	1088.2	1055.6	1013.9	966.7	914.9	860.7	817.1	811.8	808.7	
AFI OW:	ITYPE=5	CURV	o.	0.0291	0.0337	-0.0054	-0.0230	0.0343	0.0271	-0.0225	-0.0251	-0.0269	-0.0227	-0.0140	0.0425	BETAM	60.90	59.11	57.50	53.74	49.84	46.39	42.78	38.83	33.96	27.20	16.33	9.27	0.15	
STA= 15.000 MTID=183	0PTY=PT	11	٥.	_	_	_				8.40 -0		•	23.68 -(•	0- 06.9	Ħ	632.9	631.9	629.9	626.3	623.2	619.4	616.5	613.5	610.9	609.3	609.2	607.4	602.8	
	Ē	PHI	.500	.314 -(132 -0						_					Τď	23.648	24.151	24.493	25.132	25.599	25.790	25.884	25.783	25.652	25.572	25.544	25.191	24.388	
<u>.</u>	OPTX=TT	2	80	80	æ	7	7.	7	w			S.	140 4.8	4	₹	PS	18.219	18.329	18.359	8.237					16.605	16.098	15. 166	14.326	3.260	i
	61.365	7	-6.538									-6. +	-6.1	-6. 1	-6.2	BLOBLK		_	0.906								•	792 1	743	
ROTOR 1	WTF= 6	PSIC	o .	0.050	0.100	0.200	0.300	0.400	0.500	0.600	0.700	0.800	0.900	0.950	1.000	SLB		0	0		5			8		_		12 0.		

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STA 15.000 MASS AVERAGED PROPERTIES
PT= 25.358 TT= 617.70 GAMMA=1.4010 PT-RAT= 1.726 TT-RAT= 1.191
RCU= 3367.1 VM= 721.2 CZ= 701.0 MM=0.628 MABS=0.775 MREL=0.866

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0R 0 • H=0	ABH=0.	¥	0.453	0.476	0.497	0.540	0.577	0.603	0.618	0.625	0.632	0.643	0.674	0.704	0.757	MABS	0.632	0.651	. 0.668	0.705	0.738	0.762	0.781	0.797	0.816	0.847	0.911	0.960	1.047	
N ROT		ALPHAM	44.21	43.00	41.99	40:02	38.55	37.67	37.67	38.30	39.26	40.55	42.28	42.86	43.67	VABS	760.3	780.5	797.8	834.3	867.4	888.7	906.0	920.4	938.3	967.7	1031.2	1076.7	1155.9	
I 0=0+0		ე ე	530.1	532.3	533.7	536.5	540.5	543.0	553.7	570.5	593.8	629.0	693.7	732.4	798.1	MREL	0.924				_		0.826	0.788	0.748	0.712	0.695	0.709	0.758	
449	5 INBR=3	¥	545.0	570.8	593.0	639.0	678.3	703.5	717.1	722.3	726.6	735.3	762.9	789.2	836.2	VREL	1112.5	1095.1	1078.5	1052.0	1027.1	998.4	958.3	6.606	859.8	813.1	786.4	794.8	837.6	
i de	IT (PE=5	CURV		0.0184	-0.0070	-0.0384	.0571	.0619	.0664	-0.0604	-0.0447	-0.0350	-0.0050	0.0120	0.0575	BETAM	60.67	58.59	56.64	52.60	48.67	45.20	41.56	37.45	32.32	25.27	14.02	6.82	-3.36	
STA= 15.500	OPTY=PT			-0.73 0	-					9.10 -0		٠	•			11	651.1	648.7	646.2	641.3	636.8	631.9	628.4	625.5	622.9	621.0	670.9	619.6	618.3	
STAE	Ē	IHA								_	_		_			ρŢ	25.307	25.799	26.195	6.884	7.326	27.477	17.558	27.511	27.409	27.302	7.270	26.961	26.567	
9	1-16 OPTX=TT	~	4 8.500	60	2 8.129	7.	7.434	•	2 6.740	_	4 5.969				8 4.245	PS	4		4 18		19.022		421	101	.687		921	606	273	
		7	-6.334	-6.285	-6.24	-6.17	-6.1	-6.057	-6.01	-5.972	-5.924	-5.86	-5.83	-5.871	-5.95	BLOBLK			•	Ť	•	•	#	Ť			•	•	•	
ROTOR 1	WTF= 61.365	•		0.050	5. 100	0.200	006.0	0.400	0.500	0.600	0.700	0.800	0.900	0.950	1.000	פר פרט	1 0.918	2 0.9	3 0.917	6.0	5 0.914	6.0 9	7 0.906		8.0	0	11 0.8	12 0.8	13 0.8	
80	3		_	_		_		_		_	•		_	_		Ψ.														

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STA 15.500 MASS AVERAGED PROPERTIES
PT= 27.088 TT= 630.96 GAMMA=1.4008 PT-RAT= 1.843 TT-RAT= 1.216
RCU= 3819.2 VM= 696.4 CZ= 675.8 NM=0.601 MABS=0.785 MREL=0.812

H=0.	423	457	0.481	558	581	592	599	909	621	9	965 702	MARS	640	999	.685	.723	.751	.774	. 791	.807	.829	.863	710	1.048		.764														
TE ROTOR O. D*H=O O. ABH=O A! PHAN MAN	0	02.	37	200	43	. 52		9	9	57	7.95 0.	VABS	4	-	'n	0	1	6	က	<u>س</u>	0	اب ا	•		•	B MREL=0.	AXTAL	VEL R	0.622	•	0.700	0.757	0.799	0.030	0.907	0.967		1.201	1.326	1.354
D+C=0.	9	6		595.6							368.6	MREL	0.865	0.860	0.853	0.841	.824	. 803	.773	0.737	.702	674	667	0.706	;	MABS=0.798	CIENCY	POLY	0.683	ó	0.7	o o	S	o c	Ó	o	0	Ö	o,	96.0
148.43 INBR=	ų,	-	579.2	· 0	6	8 0	7		-	o (32.3 83.6	VREL	1050.5	1039.3	1026.4	1003.0	976.1	944.6	904.9	858.8	813.0	775.3	755.0	788.0		577	TT EFFI	Αο.	9	0.69	o	0 0	o 0	o o	o	Ö	Ó	0.9	ö	0.9
AFLOW= ITYPE=6 CURV		.0573	0810	1001	0060	.0708	.0502	.0271	.0191	.0603		BETAM		57.91	•			43.70		35.73		22.92 12.43	•		3ED	.3 MM=0.	204	RATI	<u>-</u>	-	-	~ •	<u>.</u>	-	-	-	-	-	-	-
STA= 16.000 MTIP=209 OPTY=PT	0	.50 -0	. .		.30 -0	.50		- 9:	.33	7.5	9 9	1	4	6	58	53	49	4	Ş.	637.7	S	633.0	č	632.3	O MASS AV	. v	ACC	RA		د	7	—`+ o o	ř	, 4	2	5	÷.	-	-	÷
STA MTII TT OI	8		727 -0						627	144	449	PT	26.560	27.120	27.560	28.390	80	Ç,	o.	29.350		29.160	. α	00	16.00	673.8	ADE SPEED		-	•	1434	4 1372.	1313	2 1195.	1132	1065	993	9	0 855	78
1=17 0PTX	131	.072	.020	.856 7	. 790 7	.732 €	9 089	624 6	. 559	537 5	675	PS	20.164	20.140	20.128	20.052	19.898	19.696	19.448	19.110	18.043	16, 780		Ň	STA	.7 VM	BLA	Z	1500.	1468	1436	1369.	1298.	1142.	1052.	952.	835.	689	93.	468.
61.365 SIC	; ;	020	\$ 5							9000		BLDBLK	•	•	•	•		•				0.930		8	7	U= 423	IVERAGE	IMM RAD	₩.	CC)	c o :	3 7.770	- 1	- φ	φ	ໝ	LD.	4.52	Ž,	3.55
ROTOR WTF= PS	0		o c				•					SL	-	7	n	7	S.	9		co (ָר ק	2 =	12	13	Ç	ž	•	PCT 1	o O	ຕ	. .	4 6	7 00	37.	46.	56.	67.	80.	88	6

E D*H=0.	ABH=O.	I	0.413	0.457	0.489	0.541	0.575	0.598	0.612	0.620	0.628	0.634	0.643	0.653	0.638	MABS	0.633	0.667	. 0.691	0.733	0.763	0.786	0.803	0.820	0.841	0.868	0.910	0.947	0.987
FRE.	•	ALPHAM	49.32	46.66	44.92	42.41	41.11	40.44	40.39	40.89	41.72	43.07	45.05	46.38	49.70	VABS	769.6	805.4	830.3	873.5	901.8	923.3	938.6	953.5	972.9	998.1	1039.0	1074.6	1113.1
_	=O ABC=O	2	583.6	585.8	586.3	589.1	593.0	598.9	608.2	624.2	647.5	681.5	735.3	777.9	848.9	MREL	0.859	0.861	0.859	0.854	0.842	0.823	0.798	0.765	0.730	0.694	0.663	0.658	0.639
4	O INBR=0	¥>	501.7	552.8	587.9	644.9	679.5	702.7	714.9	720.9	726.2	729.1	734.0	741.3	719.9	VREL	1044.7	1039.9	1032.7	1017.7	995.0	967.1	931.6	889.2	844.9	798.4	757.3	747.1	721.3
AFLOW=	ITYPE=0	CURV					-0.0459						0.1262	. 1644	. 1656	BETAM	61.30	57.89	55.30	50.68	46.93	43.40	39.89	35.84	30.74	24.05	14.25	7. 12	-3.62
STA= 17.000 MTIP=222	OPTY=FREE				.75 -0	49	13	73	.46	.51	.12 0.	.73	22.34 0.	25.96 0.	.88	Ħ	664.4	661.7	658.8	653.7	649.0	644.7	640.8	637.7	635.1	633.0	631.6	631.5	632.3
		PHI	500 0.	311 0	134 1	<u>ო</u>	179 5.			37 10	116 13	706 16			552 32	PT	26.533	27.093	27.532	28.390	28.940	29.280	29.380	29.350	29.280	29.160	28.920	28.770	28.564
1=18	OPTX=DPP	œ	80	89	80	7				6.487		ຫ	ις.	10 4	4	PS	9	•	20.014		_	_	. 204	.863	419		.903	6.144	5.319
	. 365	7	-5.700	-5.638	-5.56	-5.497	-5.42	-5.37	-5.33	-5.30	-5.29	-5.304	-5.35	-5.405	-5.520	BLOBLK	940		0.940 20		940	940	940	940 18	940 18	940 17	940 16	940 16	940 15
FREE	WTF= 61	PSIC	ö	0.050	0 100	0.200	0.300	0.400	0.500	0.600	0.700	0.800	0.900	0.950	1.000	St. Bt	-	2 0.	о 8	4	50.0	9	4	8	6	0.0	11 0.	12 0.	13 0.

HERE CONTROL OF THE PROPERTY O

STA 17.000 MASS AVERAGED PROPERTIES
PT= 28.777 TT= 643.26 GAMMA=1.4006 PT-RAT= 1.958 TT-RAT= 1.240
RCU= 4238.7 VM= 686.2 CZ= 667.6 MM=0.588 MABS=0.803 MREL=0.778

TOR	D•H=0.	ABH=0.	ĭ	0.451	0.487	0.515	0.565	0.598	0.623	0.639	0.650	0.662	0.673	0.680	0.670	0.717	MABS			٠		0.780								1.033
LE STATOR		0	ALPHAM	46.89	44.92	43.46	41.16	39.88	39.17	39.01	39.33	39.97	41.05	43.02	45.12	46.04	VABS	799.4	828.5	850.5	891.6	919.7	941.5	957.9	974.5	995.3	1022.2	1058.4	1076.9	1156.3
	D*C=0.	-4 ABC=0	5	583.6	585.0	585.0	586.7	589.6	594.7	602.9	617.6	639.3	671.2	722.1	763.2	832.3	MREL	0.880				0.866								0.717
	141.54	1 INBR=	¥>	546.3	586.7	617.3	671.3	705.8	730.0	744.4	753.7	762.9	770.9	773.8	759.9	802.6	VREL	1066.9	1060.6	1053.6	1040.7	1020.9	996. 1	964.4	926.8	887.6	847.1	803.6	769.9	802.7
	•	ITYPE=	CURV				-0.0151									. 3271	BETAM	59.20	56.42	54.13	49.83	46.25	42.87	39.48	35.58	30.75	24.49	15.64	9.28	-0.92
18.000	MT1P=235	OPTY=FREE	1	°					7.27 -0		10.56 -0	80	_	7	.71 0	.23 0	1	664.4	661.7	658.8	653.7	649.0	644.7	640.8	637.7	635.1	633.0	631.6	631.5	632.3
STA			HA	0											8 24	3 31	PT	26.533	27.093	27.532	8.390	28.940	9.280	9.380	29.350	29.280	29.160	28.920	8.770	28.564
	1=19	OPTX=DPP	~	0 8.500			2 7.831						£ 5.793		2 5.028	4	PS	5	_			19.364 2				-	•		. 660.	
	•	61.365 (7	-5.25(-5.19	-5.14	-5.062	-5.00	-4.96	-4.93	-4.93	-4.95	-5.00	-5, 108	-5.202	-5.37						0.940 19								940 14
STATOR		WTF= 61.	PSIC	o.	0.050	c. 100	0.200	0.300	0.400	0.500	0.600	0.700	0.800	0.900	0.950	÷.000	St BLD		2 0.9	3.0.9	0.0	5 0.9	6.09	7 0.9	8 0.9	9.0	10 0.9	11 0.9	12 0.9	13 0.9
ST		3																												

ASSESSED ASSESSED ASSESSED SECURIOR ASSESSED ASSESSED ASSESSED ASSESSED ASSESSED ASSESSED ASSESSED ASSESSED AS

STA 18.000 MASS AVERAGED PROPERTIES
PT= 28.777 TT= 643.26 GAMMA=1.4007 PT-RAT= 1.958 TT-RAT= 1.240
RCU= 4238.7 VM= 719.3 CZ= 700.7 MM=0.618 MABS=0.822 MREL=0.810

TOR TOR	D+H=0.	A 8H≈0.	Ī	ტ. 501	0.527	0.549	0.593	0.625	0.650	0.668	0.684	0.704	0.729	0.764	0.791	0.826	MABS	0.587	0.614	. 0.637	0.682	0.716	0.744	0.766	0.786	0.813	0.849	0.901	0.939	0.989
IN STATOR			ALPHAM	31.42	30.86	30.38	29.69	29.29	29.13	29.22	29.50	30.05	30.93	32.05	32.61	33.40	VABS	716.7	746.5	770.4	817.8	852.0	879.1	899.0	918.3	944.0	979.5	1029.9	1067.3	1115.6
	D+C=0.	# ABC=0	ე ე	373.6	382.9	389.6	405.1	416.8	428.0	438.8	452.2	472.7	503.5	546.6	575.2	614.0	MREL	1.049	1.038	1.029	1.012	0.993	0.972	0.948	0.920	0.892	0.866	0.849	0.850	0.858
	126.02	2 INBR=4	¥>	611.6	640.9	664.6	710.4	743.1	767.9	784.6	799.3	817.1	840.2	872.9	0.668	931.4	VREL	1281.7	1262.6	1245.1	1212.9	1181.3	1148.5	1112.6	1074.8	1036.5	999.3	970.0	965.4	968.0
	AFLOW=	ITYPE=2	CURV		0.0336	0.0541	.0727	.0744	9690.0	.0603	0.0514	0.0491	0.0522	0.0885	0.1161	. 1265	BETAM	61.50	59.50	57.74	54.15	51.02	48.04	45.15	41.96	37.97	32.77	25.85	21.37	15.82
19.000	MTIP=248	OPTY - BETM		0					6.61 0				31	8	-	23 0	Ħ	664.4	661.7	658.8	653.7	649.0	644.7	640.8	637.7	635.1	633.0	631.6	631.5	632.3
STA			IHd	o o							•			19.			ΡŢ	26.533	7.093	7.532	8.390	8.940	29.280	9.380	9.350	9.280	9.160	8.920	B.770	8.564
	1*20	PTX-DP	α	8.500	æ		7.866			6.957			5.918			4	PS	22		960 27	20.792 28									272 2
	-		7	-4.770	-4.723	-4.683	-4.616	-4.566	-4.531	-4.512	-4.508	-4.524	-4.565	-4.641	-4.696	-4.770													10	_
STATOR		= 61.365	PSIC		0.050	. 100	0.200	.300	0.400	. 500	.600	. 700	800	0.900	0.950	000.	ELDBLK	1 0.875	2 0.8	3 0.8	4 0.879	5 0.8	6 0.8	7 0.8	8 0.8	9.0	0.8	11 0.867	2 0.8	13 0.8
STA		WTF=		0	J	J	J	J	J	J	J	J	Ų	J	Ų		V	,										Ψ-	-	-

STA 19.000 MASS AVERAGED PROPERTIES
PT= 28.777 TT= 643.26 GAMMA=1.4005 PT-RAT= 1.958 TT-RAT= 1.240
RCU= 3076.0 VM= 777.2 CZ= 759.7 MM=0.663 MABS=0.768 MREL=0.943

ZO.	D+H=0.	ABH=O.	Ī	0.534	0.561	0.583	0.622	0.649	0.669	0.682	0.693	0.707	0.727	0.753	0.771	0.793	MABS	0.575	0.604	0.626	0.668						0.782	0.814	0.835	0.861
IN STATOR		•	ALPHAM	21.82	21.64	21.49	21.24	21.03	20.90	20.86	20.93	21.15	21.59	22.20	22.52	22.91	VABS	703.7	735.1	758.5	801.8	829.7	849.3	861.3	872.1	887.6	910.8	942.4	963.7	990.8
	D+C=0.	=4 ABC=0	3	261.6	271.1	277.8	290.4	297.8	303.0	306.7	311.5	320.2	335.1	356.1	369.1	385.7	MREL	_	1.135	_	1.108	1.089	1.067						0.924	0.917
	118.85	2 INBR=	¥	653.2	683.3	705.8	747.3	774.4	793.4	804.8	814.6	827.8	846.9	872.5	890.2	912.6	VREL	1400.1	1381.5	1363.7	1331.0	1298.6	1265.2	1229.1	1191.4	1153.2	1115.6	1080.6	1066.5	1055.2
	AFLOW=	ITYPE=2	CURV		0.0052	0.0105	0.0200	0.0268	.0322	0.0387	.0473	.0572	0.0742	0.0845	0.0978	0.1259	BETAM	62.19	60.36	58.83	55.84	53.39	51.16	49.10	46.86	44.12	40.61	36.15	33.41	30.14
20.000	=261	OPTY=BETM			67	1.34 0			59		.11	.28 0			19.55 0		11	664.4	661.7	658.8	653.7	649.0	644.7	640.8	637.7	635.1	633.0	631.6	631.5	632.3
STA	MTIP=26		H	500	341 0	186 1					691 9	54 11		_	_	_	PT	26.533	27.093	27.532	28.390	28.940	29.280	29.380	29.35C	29.280	29.160	28.920	28.770	28.564
	1=21	OPTX=DPP	~	300 8.5	∞	80	7.	7.	۲.	1	9	9	ý		ທ	ທີ	Sd	8			21.057							. 708	3.218	7.601
		61.365	2	-4.3	-4.277	-4.257	-4.2	-4.200	-4. 1	-4.174	-4.1	-4.1	-4.199	-4.233	-4.261	-4.3	BLOBLK	0.849 2	851 2	0.852 2								_	840 18	828 1
STATOR		WTF* 6	S	ö	0.050	0. 100	0.200	0.300	0.400	0.500	0.600	0.700	0.800	0.900	0.950	1 .000	St. Bi	-	0	о е	4	20	9	7	8	6	0	-	12	13

STA 20.000 MASS AVERAGED PROPERTIES

PT= 28.777 TT= 643.26 GAMMA=1.4003 PT-RAT= 1.958 TT-RAT= 1.240

RCU= 2144.6 VM= 797.1 CZ= 783.4 MM=0.675 MABS=0.725 MREL=1.035

MTP=274 AFLOW= 115 13 D+c=0. D+H=0.	STATOR					STA	STA= 21.000	_			IN STATOR	70R
61.365			Ä	22		MTIP	=274	AFLOW=		#C#		0+H+0
Z R PHI CURV VM CU ALPHAM -3.800 8.500 0. 0. 671.2 169.8 14.20 -3.800 8.346 0.56 0.0032 702.3 175.4 14.02 -3.800 8.346 0.56 0.0037 725.3 175.4 14.02 -3.800 7.621 3.59 0.0180 793.5 185.5 13.59 -3.800 7.047 6.43 0.0261 811.4 191.6 13.29 -3.800 6.107 12.22 0.0163 829.3 193.8 13.29 -3.800 6.107 12.22 0.0724 852.2 203.7 13.44 -3.800 6.107 12.22 0.0724 869.1 213.3 13.29 -3.800 5.756 14.99 0.0984 869.1 213.3 13.40 -3.800 5.750 16.64 0.1117 881.9 218.2 13.90 -3.800 5.750 16		.365	Ď	TX	-OPP	9	ry=BE					ABH=0.
-3.800 8.500 0. 0. 0. 671.2 169.8 14.20 -3.800 8.346 0.56 0.0032 702.3 175.4 14.02 -3.800 8.346 0.56 0.0057 725.3 178.9 13.86 -3.800 7.621 3.59 0.0180 793.5 189.5 13.29 -3.800 7.621 3.59 0.0180 793.5 189.5 13.29 -3.800 7.047 6.43 0.0261 811.4 191.6 13.29 -3.800 7.047 6.43 0.0261 811.4 191.6 13.29 -3.800 6.104 12.22 0.0724 869.3 193.8 13.21 -3.800 6.107 12.22 0.0724 869.1 213.9 -3.800 6.107 12.22 0.0724 869.1 213.9 -3.800 5.756 14.99 0.0984 869.1 213.3 13.79 -3.800 5.756 14.99 0.0984 869.1 213.3 13.79 -3.800 5.756 16.64 0.1117 881.9 218.2 13.90 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 18.63 0.1266 896.7 223.2 1489.9 1.216 892.3 885 -3.20092 29.390 653.7 57.61 1432.3 1.211 723.9 855 -3.20092 29.380 640.8 51.99 1333.8 1.174 815.7 858 -3.20092 29.380 640.8 51.99 1333.8 1.101 851.7 858 -3.20092 29.160 635.1 48.20 1259.3 1.0013 802.2 854 19.225 28.770 631.5 40.93 1167.3 10033 908.5	SISd		2		~	H	_	CURV	X >	5	ALPHAM	X
-3.800 8.346 0.56 0.0032 702.3 175.4 14.02 -3.800 8.196 1.13 0.0057 725.3 178.9 13.86 -3.800 7.905 2.32 0.0111 767.2 185.5 13.59 -3.800 7.621 3.59 0.0180 793.5 189.2 13.41 -3.800 7.047 6.43 0.0355 821.4 192.8 13.21 -3.800 6.748 8.10 0.0463 829.3 193.8 13.16 -3.800 6.748 8.10 0.0463 829.3 193.8 13.16 -3.800 6.707 12.22 0.0724 852.2 203.7 13.44 -3.800 6.107 12.22 0.0724 852.2 203.7 13.44 -3.800 5.756 14.99 0.0984 869.1 2.13.3 13.79 -3.800 5.376 18.63 0.1177 881.9 218.2 13.90 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 64.4 63.23 1489.9 1.216 692.3 850 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 18.63 0.1266 896.7 1.011 885.7 858 -3.800 5.350 644.7 53.66 1369.4 1.153 893.7 858 -3.20092 29.380 640.8 51.99 1333.8 1.101 851.7 858 -3.20092 29.160 633.0 45.72 1220.7 1.044 876.2 855 -3.800 5.370 631.5 40.93 1167.3 1003 908.5 852 -3.800 895 20.255 28.770 631.5 40.93 1167.3 1003 908.5	o O	ဗု	889	80	500	0		o.	671.2	169.8	14.20	0.548
-3.800 8.196 1.13 0.0057 725.3 178.9 13.86 -3.800 7.905 2.32 0.0111 767.2 185.5 13.59 -3.800 7.047 4.95 0.0261 811.4 191.6 13.29 -3.800 7.047 6.43 0.0265 821.4 191.6 13.29 -3.800 6.435 10.00 0.0583 829.3 193.8 15.16 -3.800 6.107 12.22 0.0724 852.2 203.7 13.44 -3.800 6.107 12.22 0.0724 852.2 203.7 13.44 -3.800 5.756 14.99 0.0984 869.1 213.3 13.79 -3.800 5.756 14.99 0.0984 869.1 213.3 13.79 -3.800 5.756 14.99 0.0984 869.1 213.3 13.79 -3.800 5.756 14.99 0.0984 869.1 213.3 13.79 -3.800 5.756 14.99 0.0984 869.1 213.3 13.79 -3.800 5.756 14.99 0.0984 869.1 213.3 13.79 -3.800 5.756 14.99 0.0984 869.1 213.3 13.79 -3.800 5.756 14.99 0.0984 869.1 213.3 13.79 -3.800 5.756 14.99 0.0984 869.1 213.3 13.79 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 18.63 0.1266 896.7 223.2 13.98 -3.800 5.376 64.4 63.23 1489.9 1.216 692.3 -3.800 5.376 644.7 53.66 1369.4 1.153 843.7 -3.800 640.8 51.99 1333.8 1.124 815.7 -3.800 640.8 51.99 1333.8 1.104 815.7 -3.800 640.8 51.99 1333.8 1.004 876.2 -3.800 642 52.2 29.360 635.1 48.20 1269.3 1.004 876.2 -3.800 642 632.3 38.97 1167.3 1.003 908.5 -3.800 7.005 29.160 632.0 1167.3 1003 908.5 -3.800 7.005 29.20 632.3 38.97 1153.4 0.093 924.1	0.050	۳.	800	_	.346	Ó	. 56	0.0032	702.3	175.4	14.02	0.576
-3.800 7.905 2.32 0.0111 767.2 185.5 13.59 (-3.800 7.621 3.59 0.0180 793.5 189.2 13.41 (-3.800 7.047 6.43 0.0261 811.4 191.6 13.29 (-3.800 6.748 6.10 0.00563 829.3 192.8 13.21 (-3.800 6.748 6.10 0.00583 839.4 196.9 13.20 (-3.800 6.107 12.22 0.0724 852.2 203.7 13.44 (-3.800 5.756 14.99 0.0984 869.1 213.3 13.79 (-3.800 5.756 14.99 0.0984 869.1 213.3 13.79 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.90 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.90 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.99 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.99 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.99 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.99 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.99 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.99 (-3.800 64.4 63.23 1489.9 1.216 692.3 855 21.180 28.940 644.7 53.66 1369.4 1.153 843.7 858 20.922 29.380 644.7 53.66 1369.4 1.153 843.7 858 20.922 29.380 640.8 51.99 1333.8 1.104 875.2 855 19.574 28.920 635.1 48.20 1259.3 1.004 876.2 855 19.574 28.920 635.1 48.20 1167.3 10013 894.9 855 19.574 28.920 632.3 38.97 1153.4 0.993 924.1	0.100	.3	800	w	. 196	-	13	0.0057	725.3	178.9	13.86	0.598
-3.800 7.621 3.59 0.0180 793.5 189.2 13.41 13.800 7.337 4.95 0.0261 811.4 191.6 13.29 13.21 6.43 0.0355 821.4 191.6 13.29 13.21 6.43 0.0355 821.4 192.8 13.21 6.3800 6.748 8.10 0.0463 829.3 193.8 13.16 13.800 6.435 10.00 0.0583 839.4 196.9 13.20 13.800 6.435 10.00 0.0583 839.4 196.9 13.20 13.800 5.756 14.99 0.0984 869.1 213.3 13.79 13.44 13.800 5.70 16.64 0.1117 881.9 218.2 13.90 13.800 5.376 18.63 0.1266 896.7 223.2 13.98 13.20 14.21 14.21 14.21 17.23 14.21 17.23 14.21 17.23 14.21 17.23 14.21 17.23 14.21 17.23 14.21 17.23 14.21 17.23 14.21 17.23 14.21 17.23 14.21 17.23 14.21 17.23 14.21 17.23 14.21 17.23 14.21 17.23 14.21 17.23 17.23 14.21 17.23	0.200	6-	800	1-	905	ď	.32	0.0111	767.2	185.5	13, 59	0.638
-3.800 7.337 4.95 0.0261 811.4 191.6 13.29 (-3.800 7.047 6.43 0.0355 821.4 192.8 13.21 (-3.800 6.748 8.10 0.0463 829.3 193.8 15.16 (-3.800 6.435 10.00 0.0583 829.4 196.9 13.20 (-3.800 6.435 10.00 0.0583 829.4 196.9 13.20 (-3.800 6.107 12.22 0.0724 852.2 203.7 13.44 (-3.800 5.570 16.64 0.1117 881.9 218.2 13.90 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.98 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.98 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.98 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.98 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.98 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.98 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.98 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.98 (-3.800 5.376 18.63 1.101 81.211 723.9 855 21.180 28.940 649.0 55.53 1401.8 1.174 815.7 856 21.070 29.280 644.7 53.66 1369.4 1.153 843.7 856 20.052 29.380 640.8 51.99 1333.8 1.128 843.7 855 20.052 29.380 640.8 51.99 1333.8 1.1073 865.2 855 19.574 28.920 635.1 48.20 1259.3 1.003 908.5 855 18.818 28.564 632.3 38.97 1153.4 0.993 924.1	0.300	ņ	800	-	621	m	59	0.0180	793.5	189.2	13.41	0.664
-3.800 7.047 6.43 0.0355 821.4 192.8 13.21 6.73 800 6.748 8.10 0.0463 829.3 193.8 15.16 6.3 800 6.748 8.10 0.0583 839.4 196.9 13.20 6.107 12.22 0.0724 852.2 203.7 13.44 6.3 800 5.76 14.99 0.0984 869.1 213.3 13.79 6.3 800 5.76 18.63 0.1074 869.1 213.3 13.79 6.3 849 21.366 26.53 664.4 63.23 1489.9 1.216 692.3 850 21.366 26.53 664.4 63.23 1489.9 1.216 692.3 851 21.259 28.390 653.7 57.61 1432.3 1.91 723.9 855 21.259 28.390 653.7 57.61 1432.3 1.91 789.3 855 21.070 29.280 644.7 53.66 1369.4 1.153 843.7 856 21.070 29.280 644.7 53.66 1369.4 1.153 843.7 856 20.0454 29.380 644.7 50.24 1296.8 1.107 851 29.280 637.7 50.24 1296.8 1.107 851.7 858 20.0454 29.280 637.7 50.24 1296.8 1.107 851.7 856 20.0454 29.380 640.8 51.99 1333.8 1.1073 862.2 854 19.225 29.380 635.1 48.20 1259.3 1.0073 865.2 854 19.225 29.280 635.1 48.20 1259.3 1.007 808.5 852 18.818 28.564 632.3 38.97 1153.4 0.993 924.1	0.400	6-	800	-	337	4	95	0.0261	811.4	191.6	13.29	0.683
-3.800 6.748 8.10 0.0463 829.3 193.8 13.16 (-3.800 6.435 10.00 0.0583 839.4 196.9 13.20 (-3.800 6.107 12.22 0.0724 852.2 203.7 13.44 (-3.800 5.756 14.99 0.0984 869.1 2.13.3 13.79 (-3.800 5.376 16.64 0.1117 881.9 2.18.2 13.90 (-3.800 5.376 16.64 0.1117 881.9 2.18.2 13.98 (-3.800 5.376 16.63 0.1117 881.9 2.18.2 13.98 (-3.800 5.376 16.63 0.1117 81.9 2.18.2 13.98 (-3.800 5.376 16.63 0.1266 896.7 2.23.2 13.98 (-3.800 5.376 16.63 0.1266 896.7 2.23.2 13.98 (-3.800 5.376 16.63 0.1266 896.7 2.23.2 13.98 (-3.800 5.376 66.17 61.57 1475.3 1.211 723.9 851 21.38 27.093 661.7 61.57 1475.3 1.211 723.9 852 21.259 28.940 649.0 557.51 1401.8 1.174 815.7 856 21.070 29.280 644.7 53.66 1369.4 1.153 843.7 858 20.922 29.380 640.8 51.99 133.8 1.104 875.2 858 20.0454 29.280 644.7 50.24 1296.8 1.104 876.2 858 20.0454 29.280 635.1 48.20 1259.3 1.004 876.2 855 19.574 28.920 631.5 40.93 1167.3 1.003 908.5 852 18.818 28.564 632.3 38.97 1153.4 0.993 924.1	0.500	6	800		047	9	43	0.0355	821.4	192.8	13.21	0.695
-3.800 6.435 10.00 0.0583 839.4 196.9 13.20 13.20 6.107 12.22 0.0724 852.2 203.7 13.44 13.800 5.756 14.99 0.0984 869.1 2.13.3 13.79 13.44 13.800 5.376 16.64 0.1117 881.9 218.2 13.90 13.50 5.376 18.63 0.1266 896.7 223.2 13.90 13.50 21.36 26.533 664.4 63.23 1489.9 1.216 692.3 850 21.36 26.533 664.4 63.23 1489.9 1.216 692.3 851 21.318 27.093 661.7 61.57 1475.3 1.211 723.9 853 21.259 28.940 653.7 57.61 1432.3 1.204 747.0 855 21.070 29.280 644.7 53.66 1369.4 1.153 813.7 856 20.922 29.380 644.7 53.66 1369.4 1.153 813.7 858 20.922 29.380 640.8 51.99 133.8 1.101 851.7 858 20.052 29.360 635.1 48.20 1259.3 1.001 851.7 858 20.092 29.160 633.0 45.72 1182.9 1.001 885.2 854.9 855 19.574 28.920 631.5 40.93 1167.3 1.001 895.8 852 18.518 28.554 632.3 38.97 1153.4 0.993 924.1	0.600	6	880	9	748	80	9	0.0463	829.3	193.8	13.16	0.704
-3.800 6.107 12.22 0.0724 852.2 203.7 13.44 (-3.800 5.756 14.99 0.0984 869.1 213.3 13.79 (-3.800 5.376 16.64 0.1117 881.9 218.2 13.90 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.90 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.99 (-3.800 2.376 26.533 664.4 63.23 1489.9 1.216 692.3 850 21.348 27.593 661.7 61.57 1475.3 1.211 723.9 851 21.259 28.940 653.7 57.61 1432.3 1.214 789.3 855 21.180 28.940 653.7 57.61 1432.3 1.191 789.3 855 21.070 29.280 644.7 53.66 1369.4 1.153 833.7 858 20.922 29.380 640.8 51.99 133.8 1.101 851.7 858 20.092 29.380 640.8 51.99 133.8 1.101 851.7 858 20.052 29.360 635.1 48.20 1259.3 1.0013 894.9 855 19.574 28.920 631.6 42.72 1182.9 1.0013 894.9 855 19.225 28.770 631.5 40.93 1167.3 1.0013 894.9	0.700	ņ	800	9	435	<u>ō</u>	8	0.0583	839.4	196.9	13.20	0.715
-3.800 5.756 14.99 0.0984 869.1 213.3 13.79 (-3.800 5.376 16.64 0.1117 881.9 218.2 13.90 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.98 (-3.800 5.376 18.63 0.1266 896.7 223.2 13.98 (-3.849 21.366 26.533 664.4 63.23 1489.9 1.216 692.3 851 21.348 27.093 664.7 61.57 1475.3 1.211 723.9 1.851 21.318 27.532 658.8 60.22 1460.3 1.204 747.0 1.852 21.259 28.390 653.7 57.61 1432.3 1.191 789.3 1.852 21.070 29.280 644.7 57.61 1432.3 1.191 789.3 1.858 20.092 29.380 640.8 51.89 1333.8 1.101 851.7 853 20.092 29.160 635.1 48.20 1259.3 1.001 851.7 858 20.092 29.160 635.1 48.20 1167.3 1.003 908.5 852 18.818 28.56 632.3 38.97 1153.4 0.993 924.1	0.800	e P	800	ý	107	12.	22	0.0724	852.2	203.7	13.44	0.729
-3.800 5.570 16.64 0.1117 881.9 218.2 13.90 (1.28.2)	0.900	ņ	800	ທ	756	14.	66	0.0984	869.1	213.3	13.79	0.746
BLUBLK PS PT TT BETAM VREL MREL VABS 0.849 21.356 26.533 664.4 63.23 1489.9 1.216 692.3 0.850 21.336 26.533 664.4 63.23 1489.9 1.216 692.3 0.850 21.336 26.533 664.4 63.23 1489.9 1.216 692.3 0.851 21.318 27.592 658.8 60.22 1460.3 1.204 747.0 0.853 21.259 28.390 653.7 57.61 1475.3 1.204 747.0 0.855 21.180 28.940 649.0 55.53 1401.8 1.174 815.7 0.856 21.070 29.280 644.7 53.66 1369.4 1.153 833.7 0.858 20.723 29.380 640.8 51.99 1333.8 1.128 843.7 0.858 20.723 29.380 640.8 51.99 1333.8 1.1073 862.2 0.858 20.0454 29.280 635.1 48.20 1259.3 1.073 862.2 0.854 19.225 28.770 631.5 40.93 1167.3 1.003 908.5 0.854 19.225 28.770 631.5 40.93 1167.3 1.003 908.5 0.855 18.818 28.564 632.3 38.97 1153.4 0.993 924.1	0.950	6	800	'n	570	16.	64	0.1117	881.9	218.2	13.90	0.758
BLDBLK PS PT TT BETAM VREL MREL VABS 0.849 21.366 26.533 664.4 63.23 1489.9 1.216 692.3 0.850 21.343 27.093 661.7 61.57 1475.3 1.211 723.9 0.851 21.348 27.532 658.8 60.22 1460.3 1.214 723.9 0.853 21.259 28.390 653.7 57.61 1432.3 1.191 789.3 0.855 21.070 29.280 644.7 53.66 1369.4 1.153 815.7 0.856 21.070 29.280 640.8 51.39 1333.8 1.128 843.7 0.858 20.723 29.350 640.8 51.39 1.073 862.2 0.858 20.044 29.280 635.1 48.20 1.044 876.2 0.855 19.574 28.90 635.0 45.72 1220.7 1.044 876.2 0.854 19.	1.000	က်	800	ຜ	376	≅	63	0. 1266	896.7	223.2		0.772
0.849 21.366 26.533 664.4 63.23 1489.9 1.216 692.3 0.850 21.343 27.093 661.7 61.57 1475.3 1.211 723.9 0.851 21.348 27.532 658.8 60.22 1460.3 1.204 747.0 0.853 21.259 28.390 653.7 57.61 1432.3 1.191 789.3 0.855 21.180 28.940 649.0 55.53 1401.8 1.174 815.7 0.856 21.070 29.280 644.7 53.66 1333.8 1.128 843.7 0.858 20.092 29.380 640.8 51.99 1333.8 1.101 851.7 0.859 20.742 29.380 637.7 50.24 1296.8 1.101 851.7 0.858 20.092 29.160 633.0 45.72 1182.9 1.015 894.9 0.855 19.574 28.920 631.6 42.72 1182.9 1.003 908.5 0.852 18.818 28.564 632.3 38.97 1153.4 </td <td></td> <td>BLK</td> <td>PS</td> <td></td> <td>۵</td> <td>;</td> <td>11</td> <td>BETAM</td> <td>VREL</td> <td>MREL</td> <td>VABS</td> <td>MABS</td>		BLK	PS		۵	;	11	BETAM	VREL	MREL	VABS	MABS
0.850 21.343 27.093 661.7 61.57 1475.3 1.211 723.9 0.851 21.318 27.532 658.8 60.22 1460.3 1.204 747.0 0.853 21.259 28.390 653.7 57.61 1432.3 1.191 789.3 0.855 21.180 28.940 649.0 55.53 1401.8 1.174 815.7 0.856 21.070 29.280 644.7 53.66 1369.4 1.153 833.7 0.858 20.092 29.380 640.8 51.99 1333.8 1.101 851.7 0.859 20.723 29.380 637.7 50.24 1296.8 1.101 851.7 0.858 20.092 29.160 635.1 48.72 1220.7 1.044 876.2 0.855 19.574 28.920 631.6 42.72 1182.9 1.015 894.9 0.854 19.225 28.770 631.5 40.93 1167.3 1.003 908.5 0.852 18.818 28.564 632.3 38.97 1153.4 </td <td># O.8</td> <td>149</td> <td>21.3</td> <td>99</td> <td>26.</td> <td>533</td> <td>664.4</td> <td>63.23</td> <td>1489.9</td> <td>1.216</td> <td>692.3</td> <td>0.565</td>	# O.8	149	21.3	99	26.	533	664.4	63.23	1489.9	1.216	692.3	0.565
0.851 21.318 27.532 658.8 60.22 1460.3 1.204 747.0 0.853 21.259 28.390 653.7 57.61 1432.3 1.191 789.3 0.855 21.180 28.940 649.0 55.53 1401.8 1.174 815.7 0.856 21.070 29.280 644.7 53.66 1369.4 1.153 833.7 0.858 20.092 29.380 640.8 51.39 133.8 1.108 843.7 0.858 20.0454 29.380 635.1 48.72 1296.8 1.101 851.7 0.858 20.092 29.160 635.1 45.72 1220.7 1.044 876.2 0.855 19.574 28.920 631.6 42.72 1182.9 1.003 908.5 0.854 19.225 28.770 631.5 40.93 1167.3 1.003 908.5 0.852 18.818 28.564 632.3 38.97 1153.4 0.993 924.1	2 0.8	150	21.3	133	27.	093	661.7	Ī	1475.3	1.211	723.9	0.594
0.853 21.259 28.390 653.7 57.61 1432.3 1.191 789.3 0.855 21.180 28.940 649.0 55.53 1401.8 1.174 815.7 0.856 21.070 29.280 644.7 53.66 1369.4 1.153 833.7 0.858 20.723 29.380 640.8 51.99 1333.8 1.128 843.7 0.858 20.0454 29.280 635.1 48.72 1259.3 1.073 862.2 0.858 20.092 29.160 635.1 48.72 1220.7 1.044 876.2 0.855 19.574 28.920 631.6 42.72 1182.9 1.065 894.9 0.854 19.225 28.770 631.5 40.93 1167.3 1.003 908.5 0.852 18.818 28.564 632.3 38.97 1153.4 0.993 924.1	3 0.8	51	21.3	18	27.	532	658.8			1.204	747.0	.0.616
0.855 21.180 28.940 649.0 55.53 1401.8 1.174 815.7 0.856 21.070 29.280 644.7 53.66 1369.4 1.153 833.7 0.858 20.922 29.380 640.8 51.99 1333.8 1.128 843.7 0.858 20.723 29.280 635.1 48.20 1259.3 1.073 862.2 0.858 20.0454 29.160 635.1 48.20 1220.7 1.044 876.2 0.855 19.574 28.920 631.6 42.72 1182.9 1.015 894.9 0.854 19.225 28.770 631.5 40.93 1167.3 1.003 908.5 0.852 18.818 28.564 632.3 38.97 1153.4 0.993 924.1		53	21.2	29	28.	390	653.7			1.191	789.3	0.656
0.856 21.070 29.280 644.7 53.66 1369.4 1.153 833.7 0.858 20.922 29.380 640.8 51.99 1333.8 1.128 843.7 0.858 20.723 29.280 637.7 50.24 1296.8 1.101 851.7 0.858 20.0454 29.280 635.1 48.20 1.073 862.2 0.855 19.574 28.920 631.6 45.72 1182.9 1.043 876.2 0.854 19.225 28.770 631.5 40.93 1167.3 1.003 908.5 0.852 18.818 28.564 632.3 38.97 1153.4 0.993 924.1		52	21.1	80	28.	940	649.0			1.174	815.7	0.683
0.858 20.922 29.380 640.8 51.99 133.8 1.128 843.7 0.858 20.723 29.350 637.7 50.24 1296.8 1.101 851.7 0.859 20.454 29.280 635.1 48.20 1259.3 1.073 862.2 0.855 19.574 28.9160 633.0 45.72 1182.9 1.044 876.2 0.854 19.225 28.770 631.5 40.93 1167.3 1.003 908.5 0.852 18.818 28.564 632.3 38.97 1153.4 0.993 924.1		26	21.0	20	29.	280	644.7			1.153	833.7	0.702
0.858 20.723 29.350 637.7 50.24 1296.8 1.101 851.7 0.859 20.454 29.280 635.1 48.20 1259.3 1.073 862.2 0.858 20.092 29.160 633.0 45.72 1220.7 1.044 876.2 0.855 19.574 28.920 631.6 42.72 1182.9 1.015 894.9 0.854 19.225 28.770 631.5 40.93 1167.3 1.003 908.5 0.852 18.818 28.564 632.3 38.97 1153.4 0.993 924.1		58	20.9	22	29.	380	640.8		·	1.128	843.7	0.714
0.859 20.454 29.280 635.1 48.20 1259.3 1.073 862.2 0.858 20.092 29.160 633.0 45.72 1220.7 1.044 876.2 0.855 19.574 28.920 631.6 42.72 1182.9 1.015 894.9 0.854 19.225 28.770 631.5 40.93 1167.3 1.003 908.5 0.852 18.818 28.564 632.3 38.97 1153.4 0.993 924.1		58	20.7	23	29.	350	637.7		1296.8	1.101	851.7	0.723
0.858 20.092 29.160 633.0 45.72 1220.7 1.044 876.2 0. 0.855 19.574 28.920 631.6 42.72 1182.9 1.015 894.9 0. 0.854 19.225 28.770 631.5 40.93 1167.3 1.003 908.5 0. 0.852 18.818 28.564 632.3 38.97 1153.4 0.993 924.1 0.		59	20.4	54	29.	280	635.1		1259.3	1.073	862.2	0.734
0.855 19.574 28.920 631.6 42.72 1182.9 1.015 894.9 0. 0.854 19.225 28.770 631.5 40.93 1167.3 1.003 908.5 0. 0.852 18.818 28.564 632.3 38.97 1153.4 0.993 924.1 0.		58	20.0	95	29.	160	633.0		1220.7	1.044	876.2	0.749
0.854 19.225 28.770 631.5 40.93 1167.3 1.003 908.5 0. 0.852 18.818 28.564 632.3 38.97 1153.4 0.993 924.1 0.		55	19.5	74		920	631.6		1182.9	1.015	894.9	0.768
0.852 18.818 28.564 632.3 38.97 1153.4 0.993 924.1 0.		54	•	25		770	631.5		1167.3	1.003	908.5	0.781
		25		₩	•	564	632.3	38.97	1153.4	0.993	924.1	0.796
			מ	7	3		つつせ	MASS AVERAGED PROPERTIES	7777	/		

THE POSSESSED OF THE PROPERTY OF THE PROPERTY

STA 21.000 MASS AVERAGED PROPERTIES
PT= 28.777 TT= 643.26 GAMNA=1.4003 PT-RAT= 1.958 TT-RAT= 1.240
RCU= 1351.4 VM= 809.4 CZ= 799.1 MM=0.683 MABS=0.703 MREL=1.119

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STA 22.000 MASS AVERAGED PROPERTIES
PT= 28.777 TT= 643.26 GAMMA=1.4002 PT-RAT= 1.958 TT-RAT= 1.240
RCU= 653.6 VM= 798.7 CZ= 791.5 MM=0.672 MABS=0.676 MREL=1.184

0R	D•H=0.		0.536		0.577	•	0.042	0.671				•	0.708	0.697	MABS	•	•		0.616	0.642	0.660	•	0.678				•		()()	MREL= 1.244					_									
E STA	- ,	AL PHAM		o.						o.	c;	Ö	o.	o.	VABS	658.1	685.2	702.8	744.8	770.2	788.1	4.767	203.7	831.5	831.5	831.7	820.0			-KAIE I	AXIAL	VEL R	1.205	-	-	-	•	·· •	- •		-	1, 135	1.184	1.171
•	0.C=0.				ö					o.	٥.	o.	ö	o.	MREL	. 333	.330	. 323		. 299	.280	922.		179	143	. 124	.095		*	. 65	EFFICIENCY	POLY	0.663	0.696	0.723	0.785	0.834	0.877	9.00	0.930	0.968	0.949	. 92	0.887
ļ	8.17 TNDD-4	•	· -	.2	æ. ⟨	æ. (7 -		· - .	7	S	ž.		o.	VREL	<u>-</u>	.2	9	თ. (N (<u> </u>	٥		σ	0		38.4	AVEDAGEN DONDEDTIES		- X	EFFIC	AD.	3			0.765		0.865		0.942		94	6.	.87
•	֚֚֚֝֟֝֝֡֝֝֝֟֝֝֡֡֝֝֡֡֝֡֡֝֡֡֝֡֡֡֡֡֡֝֡֡֡֝֡֡	? >	658	685.	702	744	7 20	707	803	811	31	*	3	820.	AM VE	_							49 1454			ıc T		בים מים	ביים ביים	M=0.657	ACC 1T	RATIO	. 2809	.2757	. 2701	. 2603	.2512	. 2429	4007	2294	220	.2177	-	.2190
	AFLOW«	2		0.0063	0.0091	•	0.0184			0.0656	٠.	0.1249	. 13	0. 1267	BET.		65	64	62.	9	. 28	70	10 A	האלי	5			AVEDAG	A C C C C C C C C C C C C C C C C C C C	8.4.8 2.4.8	Ρ	01	**	_	-	1.8870 1	_	9488	- •		-	9223 1	957 1	480 1
STA= 23.000	1P=300	11-051	۔	.50		69.	9 6		25	.46	.03	.89	.80	.52	11	664.4	661.7	658.8	653.7	649.0	644.7	640.8	637.	633	631.6	•	n	MACC	•	GAMMA=1 CZ= 77	ACC	œ	1.7	æ. -	-	4.8	5 .		n (הים			±.	1 .
	Ξ					- (9 6	7	מי	9	80	o	₽	*	Г	•	26.581	26.910	7.731	8.269	•	28.781	28.759	28.85	8.250	7.86	7.15	C	۶ ۱	. 26 82.6	SPEED													
į	1*24 201*-000	֝֡֝֝֡֝֝֝֡֝֝֝֓֞֝֝֓֓֓֓֓֞֝֓֓֓֓֓֡֡֓֓֓֓֓֓֓֓֡֡֓֓֓֡֡֡֡֡֓֓֡֓֡֡֡֡֡֡֡֓֓֡֡֡֓֡֡֡֡	∞.	œ	&	٠. ١	- 1		. ග	9	9	ໝ່	B	ស	S	481								667	220	•	635	CTA 2		TI = 643 VM = 7	BLADE	Z												
(0 605.	-2.567		-2.595							-2.816	•	•	r P	21.	2	5	7	2	2	7	7 6	א ה	3 8	5	19		ç	163	ıu.	RAD	.500	340	. 186	.889	.601	.314	120.	30.4	042	648	419	137
OR	ď	7 0) 5	050	8				0.600				950	8	BLDBLK	0	o	o	o	0.940	o (o (o (o c	-	o	o			P1 = 28. RCU=	AVERAGE	IMM R	80	80	œ	7	-	- 1	٠ (ט פ	•	ທີ	ß.	
STATOR	7		o.		o ·	0	o 0	ċċ	ó	Ö	0	ö	•	-	SŁ	-	8	က	4	ស (91	~ 6	20 0	. .	? =	12	13		Č	ΣŒ		PCT	0	4	o	48	56	32	4 7	200	73	84.8	9	5

THE CONTRACTOR ASSESSMENT CONTRACTOR ASSESSMENT ASSESSMENT ASSESSMENT PROJECTION BROADERS SECTION ASSESSMENT OF THE PROJECTION OF THE PROJ

E D+H=0.	ABH=0.	Ĭ	0.551	0.575	0.592	0.631	0.658	0.678	0.690	0.698	0.709	0.728	0.726	0.724	0.711	MABS	0.551	0.575	0.592	0.631	0.658	0.678	0.690	0.698	0.709	0.728	0.726	0.724	0.711
FRE		LPHAM							ö				ó	ö	ö	VABS	675.7	702.4	719.7	761.5	787.9	807.1	817.9	824.8	834.8	854.0	850.7	848.6	835.5
D+C=(O ABC=D.	- -	ó	ö	ó	o O	ö	ó	ö	ó	ö	ó	ö	o O	ö	MREL	1.341	1.338	1.332	1.325	1.312	1.295	1.273	1.248	1.223	1.204	1.168	1.148	1.120
116.57		T >	675.7	702.4	719.7	761.5	787.9	807.1	817.9	824.8	834.8	854.0	850.7	848.6	835.5	VREL	1645.2	1634.2	1620.3	1598.3	1571.6	1542.7	1509.9	1474.6	1440.7	1412.1	1368.9	1346.1	1315.4
AFLOW=	ITYPE=0	CURV		_	_				0.0402		0.0644	0.0793		0.1151	. 1260	BETAM	65.75	64.55	63.63	61.54	59.91	58.45	57.20	55.99	54.59	52.79	51.58	50.92	50.56
STA= 24.000 MTIP=313	REE			32	0.63 0	. 18	.68	. 16 0	.64	. 13	.63	.11		.85	.28 0	11	664.4	661.7	658.8	653.7	649.0	644.7	640.8	637.7	635.1	633.0	631.6	631.5	632.3
		PHI	500 0.	361 0.	226 0	-	•	450 2	7	n	54 3	373 4	•	4	.	μ	26.109	26.581	26.910	27.731	28.269	28.639	28.781	28.769	28.750	28.851	28.250	27.860	27.159
1=25	OPTX=DPP	œ	œ	∞.	&	۲.	_	7.			0 6.654			X 5.921		PS	47	. 244	. 236	. 203	145		•	20.778				19.652	.381
	61.365	7	-2.000	-2.8	-2.8	-2.00	-2.00	-2.8	-2.000	-2.8	-2.000	-2.000	-2.00	-2.000	-2.000	BLDBLK	0.950 21	0.950 21	0.950 21								_		
EXIT	WTF= 61	PSIC	ö	0.050	o. 180	0.200	0.300	0.400	0.500	0.600	0.700	0.800	006.0	0.950	1.000	SLBL		2	о 8	•	5	9	7 0.	8		0	-	12 0.	13 0.

ANDER REPORTED LA SECUE DE L'ESSENTATION LE RECENSE DE SECUES DE SECUES DE L'ESSENTATION DE L'ESSENTATION DE L

STA 24.000 MASS AVERAGED PROPERTIES PT= 28.163 TT= 643.26 GAMMA=1.4002 PT-RAT= 1.916 TT-RAT= 1.240 RCU= 0. VM= 801.9 CZ= 800.8 MM=0.674 MABS=0.674 MREL=1.261

The second contract of the second contract of

E D+H=0.	ABH=0.	¥	0.566	0.590	0.606	0.644	0.668	0.686	0.696	0.700	0.706	0.718	0.705	0.695	0.676	MABS	0.566	0.590	,			Q. 686	969.0	0.700	0.706		0.705	0.695	0.676
FRE	٥.	ALPHAM	oʻ	o	Ċ	o O	ó	ó	ö	ö	ó	oʻ	o'	ó	ö	VABS	693.1	718.8	735.5	775.4	799.8	816.7	824.4	827.3	831.7	843.1	828.0	817.6	798.1
D*C=0.		Ş	oʻ	o.	ó	o.	o.	ó	o.	ó	ö	o	ó	ó	ö	MREL	1.349	1.347	1.341	1.334	1.320	1.303	1.280	1.253	1.225	1.201	1.157	1.132	1.099
116.27	O INBR-0	X >	693.1	718.8	735.5	775.4	8.667	816.7	824.4	827.3	831.7	843.1	828.0	817.6	798.1	VREL	1652.4	1641.8	1628.3	1606.6	1580.0	1550.7	1516.9	1480.1	1443.3	1410.2	1359.7	1331.6	1296.6
AFLOW=		CURV	٥.	0.0025	0.0048	0.0092	0.0136	0.0181	0.0229	0.0280	0.0335	0.0398	0.0464	0.0493	. 1263	BETAM	65.20	64.03	63, 15	61.14	59.59	58.22	57.08	56.01	54.81	53.28	52.49	52.12	52.01
STA= 25.000 MTIP=326	OPTY=FREE	PHI		O. 19 C	0.36	0.66 0	0.91	1.13 0	1.32 0	1.47 C	1.58 0	1.62 0	1.54 0	1.41 0	0.00	Ħ	664.4	661.7		653.7	649.0	644.7	_	_	635.1	633.0	631.6	631.5	632.3
STA		o:	500	365	232			7.470	216	6.954	6.684	406	6.112	5.956	790	P	26.109	26.581	26.910	27.731	28.269	28.639	28.781	28.769	28.750	28.851	28.250	27.860	27.159
I = 26		2	.270 8	.270 8.	.270 8.	.270 7.	. 270 7	.270 7.	.270 7.	.270 6.	.270 6.	.270 6.	.270 6.	.270 5.	.270 5.	S d	21.014	21.012	21.006	20.986	20.950	20.898	20.827	20.734	20.615	20.466	20.280	20.173	19.989
	61.365	ပ	-	-	÷ Ω	- 0	7	٠ و	-	τ ·	-	-	- 0	- 0	- 1	BLOBLK	0.956	0.956	0.956	0.956	0.956	0.956	926.0	0.956	0.956	0.956	0.956	•	0.956
EXIT	WTF=	PSIC	ö	0.050	o. 100	0.200	0.300	0.400	0.500	0.600	0.700	0.800	0.900	0.950	-000	SL	-	8	ო	4	រភ	9	7	œ	(A	ç	-	5	1 3

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Land But the State of the Control of the State of the Sta

STA 25.000 MASS AVERAGED PROPERTIES
PT = 28.163 TT = 643.26 GAMMA = 1.4002 PT - RAT = 1.916 TT - RAT = 1.240
RCU = 0. VM = 803.2 CZ = 803.0 MM = 0.675 MABS = 0.675 MREL = 1.264

	!									
	EXIT	1-27	STA	STA= 26.000 MT10-230	AE1 OW:	416 28	C#C#	FREE	□•H±0	
	WTF= 61,365			OPTY=FREE		O INBR=0		YB (ABH=O.	
	- 13	7		IHd	ຽ	Z.	2	ALPHAM	.	
	o o	50 8.	8	0		711.0	0		0.581	
	0.050	350 8.			8	735.8			0.605	
	0. 100	60				751.6	0		0.620	
	0.50	350 7				789.3			0.656	
	0.300	350 7				811.0			0.679	
	0.400	350				824.4			0.693	
	0.500	350				827.9			0.699	
	0.600					825.4	0.		. 869.0	
	0.700	350				822.9			0.698	
	0.800	Ψ				825.8			0.702	
	0.900	350 6				799.3			0.678	
	0.950	.350	5.961 -0	-0.10 -0	0000	781.7	°.		0.662	
	1.000			°		748.9			0.631	
	SL BLDBLK	BLK PS	PT	Ħ	BETAM	VREL	MREL	VABS	MABS	
	_	20	26.109	664.4	64.64	1660.0	80	711.0	0.581	
	2 0.95	956 20.768	26.581	661.7	63.51	1649.7	-	735.8	0.605	
	o	20.	26.910	658.8	62.65	1636.3		751.6	0.620	
	Ö	0	27.731	653.7	60.73	1614.5	1.342 7	789.3	0.656	
	Ö	20.	28.269	649.0	59.27	1587.2	_	611.0	0.679	
	Ö	20.	28.639	644.7	58.02	1556.6	on.	_	0.693	
4	Ö		28.781	640.8	57.02	1520.8	*	_	0.699	
0	o	20.	28.769	637.7	56.13	1481.0	 (D)		0.698	
	Ö	20.	28.750	635.1	55. 15	1440.3	_	_	0.698	
	0	50.	28.851	633.0	53.90	1401.6		_	0.702	
	Ö	956 20.765	28,250	631.6	53.50	1343.6	ത	e,	0.678	
	•	2	•	631	53.38	1310.6	6	781.7	0.662	
	ö	20.	27.159	632	53.76	1266.9	1.068 7	748.9	0.631	

STA 26.000 MASS AVERAGED PROPERTIES
PT= 28.163 TT= 643.26 GAMMA=1.4002 PT-RAT= 1.916 TT-RAT= 1.240
RCU= 0. VM= 801.4 CZ= 801.3 MM=0.573 MASS=0.673 MREL=1.263

Phase I Rotor

entropy established besteered verteered out the court of the court of

BLADE FORCES

THE FORCE CALCULATIONS ARE 'PER BLADE ROW'.
TO FIND THE FORCE ON A SINGLE BLADE, DIVIDE BY 'NB'

THE FORCES ARE THAT OF THE AIR ON THE BLADES.
POSITIVE AXIAL IS AFT; POSITIVE TANGENTIAL IS IN ROTATION DIRECTION.
THE COLUMNS HEADED BY F-TAN*, F-AXL*, AND F-RAD* ARE THE TANGENTIAL,
AXIAL, AND RADIAL FORCES PER INCH OF CHANGE IN R-AVG.

0 -	9	+	2	7	42.	•	19.	13.	16.	16.	17.	23.	28.
F-AXL*	388.6	392.	397.	394.	378.	355.	325.	292.	254.	287.	139.	86.	47.
Z-	m	383.	308.	389.	387.	300.	289.	276.	264.	246.	214.	187.	166.
H-AVG		B. 185	'n	۲.	æ	7	æ	ω.		ო	6.	რ.	6.
R-AVG	5.0	.31	. 13	.77	. 48	.82	.62	. 19	.71	.18	.52	.18	. 55
SF	,-4	8	ო	◄	ហ	9	7	∞	6			12	

NET TORQUE = -8Ø81.5 IN-LB
NET TAN. FORCE = -129Ø.7 LB
NET AXIAL FORCE = -1289.8 LB
NET RADIAL FORCE = -99.3 LB

2. STREAMSURFACE BLADE COORDINATES

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Figure 30 shows the stacked Phase I rotor streamsurface sections.

Each page of the following tabulation gives the coordinates for one of these sections. The streamline designation for these sections corresponds to the calculation streamlines of the circumferential average flow calculation.

Streamline 1 is at the casing and streamline 13 is at the hub. Also given in the tabulations are coordinates for the section meanline, the meanline angle, and the section thickness at each point. Streamsurface section chord, camber angle, and stagger angle are also given. All dimensions in this tabulation are in inches or degrees.

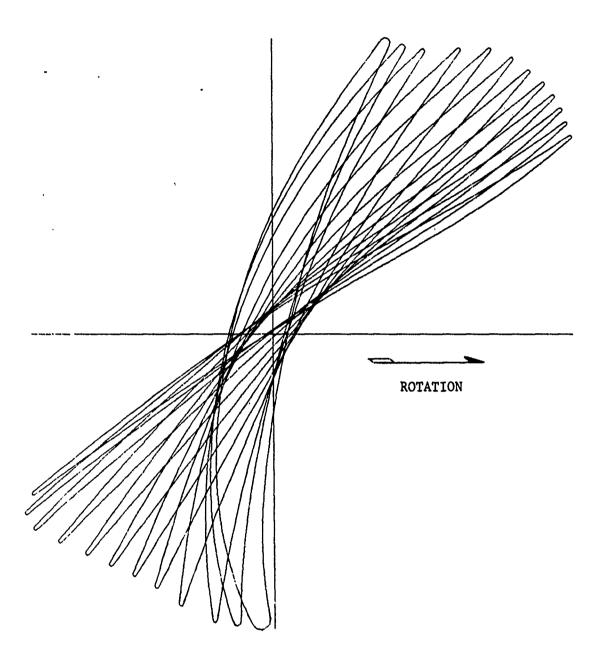


Figure 30. Stacked Phase I Rotor Streamsurface Sections

NB 20

MERIDIONAL AIRFOIL GEOMETRY - STREAMLINE

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	B • M 1 (M)	2	ΡŢ	xS	٨S	۵×	dλ
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- 26	877 0.	188	៖ ហ	-1.04247	1.63448	-1.01178	1.65571
-57	.664 0.	121	9	.9952		-0.95718	1.58330
ភ	.443 0.	184	7	-0.94791	1.47893	-0.90279	1.50837
ų,	.201 0.	379	c	-0.90032	1.39810	-0.84861	1.43084
7	.920 0.	904	6	-0.85248	1.31510	-0.79467	1 35061
Ť	.696	141	õ	-0.80438	1.22985	-0.74100	1.26763
Ť	.332 0.	173	Ξ	-0.75600	1.14232	-0.68760	1, 18 193
ĭ	.762 0.	505	72	-0.69754	1.03433	-0.62393	•
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9	.853 0.	999	74	-0.57914	•	-0.49807	•
9	.556 0.	517	5	-0.51915		-0.43593	
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່ເນ	ö	358	18	-0.33632	0.35489	-0.25237	0.40130
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ij	o	314	22	-0.08807	-0.06422	-0.01210	-0.01753
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ĭ	Ö	578	24	0.03699			
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			37	0.84626	-1.38348	0.86516	-1.36947
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77000 0.50612 -0.83083 -53.599 0.06096 28 0.34419 -0.66935 0.40134 -0. 80000 0.57280 -0.92086 -53.343 0.05584 29 0.41285 -0.75950 0.46604 -0. 810000 0.70646 -1.00996 -53.024 0.05588 30 0.48159 -0.034892 0.53066 -0. 81000 0.7064 -1.18445 -52.129 0.03980 32 0.61928 -1.02517 0.5969 -0. 81000 0.77284 -1.18445 -52.129 0.03980 32 0.61928 -1.02517 0.5969 -0. 81000 0.77284 -1.18445 -52.129 0.03435 33 0.68820 -1.1164 0.72413 -1. 81000 0.90620 -1.36930 -51.529 0.03435 33 0.68820 -1.1164 0.72413 -1. 81000 0.90620 -1.35221 -50.835 0.02892 34 0.75714 -1.19667 0.78855 -1. 810000 0.96177 -1.41967 -50.199 0.02444 35 0.85608 -1.27999 0.85297 -1. 8100000 1.01734 -1.48557 -49.526 0.01999 36 0.89500 -1.36134 0.91741 -1. 8100000 1.01734 -1.48557 -49.526 0.01999 30 1.00932 -1.487793 1.02093 -1. 81000000 -1.01734 -1.48757 1.01734 -1.	0			ö	53.		27	0.27561	-0.57849	0.33656	-0.53451
80000 0.57280 -0.92086 -53.343 0.05584 29 0.41285 -0.75950 0.46604 -0. 81000 0.63948 -1.00996 -53.024 0.05058 30 0.48159 -0.84892 0.53066 -0. 81000 0.70616 -1.00991 -52.624 0.004522 31 0.55041 -0.03753 0.59520 -0. 81000 0.70616 -1.18445 -52.129 0.03980 32 0.65820 -1.02517 0.65969 -0. 81000 0.83952 -1.26930 -51.529 0.03435 33 0.68820 -1.11164 0.72413 -1. 81000 0.90620 -1.35221 -50.835 0.02892 34 0.75714 -1.19667 0.78855 -1. 81000 0.90617 -1.41967 -50.199 0.02444 35 0.82608 -1.27999 0.85297 -1. 81000 0.96177 -1.41967 -50.199 0.02444 35 0.82608 -1.27999 0.85297 -1. 810000 1.01734 -1.48557 -49.526 0.01999 36 0.89500 -1.36134 0.91741 -1. 81000 0.96720 -1.48557 -49.526 0.01999 36 0.89500 -1.48749 0.97116 -1. 81000 0.96720 -1.48557 -49.526 0.01999 36 0.89500 -1.48749 0.97116 -1. 81000 0.96720 -1.48757 1.01734 -1.	0			ö	•	•	28	0.34419	-0.66935	0.40134	
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86000 0.70616 -1.09791 -52.624 0.04522 31 0.55041 -0.93753 0.59520 -0.93753 0.59520 -0.907284 -1.02517 0.65969 -0.9000 -0.65969 -1.02517 0.65969 -0.92800 -0.65969 -0.9000 -0.72413 -1.1164 0.72413 -1.1166 -1.1176 -1.1166 -1.1176 -1.1166 -1.1176 -1.1166 -1.1166 -1.1166 -1.1166 -1.1166 -1.1166 -1.1166 -1.1166 -1.1166 -1.1166 -1.1166 -1.1166 -1.1166 -1.1166 -1.1166 -1.1166 -1.1166 -1.1166 <td>0</td> <td>œ</td> <td></td> <td>÷.</td> <td>-53.024</td> <td>•</td> <td>30</td> <td>0.48159</td> <td>-0.84892</td> <td>0.53066</td> <td>-0.81274</td>	0	œ		÷.	-53.024	•	30	0.48159	-0.84892	0.53066	-0.81274
89000 0.77284 -1.18445 -52.129 0.03980 32 0.61928 -1.02517 0.65969 -0. 92000 0.83952 -1.26930 -51.529 0.03435 33 0.68820 -1.11164 0.72413 -1. 95000 0.90620 -1.35221 -50.835 0.02892 34 0.75714 -1.19667 0.78855 -1. 97500 0.96177 -1.41967 -50.199 0.02444 35 0.82608 -1.27999 0.85297 -1. 00000 1.01734 -1.48557 -49.526 0.01999 36 0.89500 -1.36134 0.91741 -1. 37 0.98500 -1.36134 0.91146 -1. 38 1.000305 -1.48462 1.01866 -1. 39 1.00932 -1.48793 1.02093 -1.	0			÷.		٠	31	0.55041	-0.93753	0.59520	-0.90420
.92000 0.83952 -1.26930 -51.529 0.03435 33 0.68820 -1.11164 0.72413 -1. 95000 0.90620 -1.35221 -50.835 0.02892 34 0.75714 -1.19667 0.78855 -1. 95000 0.96177 -1.41967 -50.199 0.0244 35 0.82608 -1.27999 0.85297 -1. 000000 1.01734 -1.48557 -49.526 0.01999 36 0.89500 -1.36134 0.91741 -1. 37 0.95238 -1.42749 0.97116 -1. 38 1.000305 -1.48462 1.01866 -1. 39 1.00932 -1.48793 1.02093 -1.	0			÷.			32	0.61928	٠	0.65969	•
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97500 0.96177 -1.41967 -50.199 0.02444 35 0.82608 -1.27999 0.85297 -1. 00000 1.01734 -1.48557 -49.526 0.01999 36 0.89500 -1.36134 0.91741 -1. 37 0.95238 -1.42749 0.97146 -1. 38 1.00305 -1.487793 1.01866 -1. 39 1.00932 -1.48793 1.02093 -1.	0		•	-1.35221			34	•	-1.19667	0.78855	-1.17224
00000 1.01734 -1.48557 -49.526 0.01999 36 0.89500 -1.36134 0.91741 -1. 37 0.95238 -1.42749 0.97116 -1. 38 1.00305 -1.48462 1.01866 -1. 39 1.00932 -1.48793 1.02093 -1. 40 1.01734 -1.48557 1.01734 -1.	0	.97500	•	-1.41967	<u>.</u>	.0244	32	•	-1.27999	0.85297	-1.25862
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1,00305 -1,48462 1,01866 -1. 1,00932 -1,48793 1,02093 -1. 1,01734 -1,48557 1,01734 -1.							37	•	-1.42749	0.97116	-1.41185
1.00932 -1.48793 1.02093 -1. 1.01734 -1.48557 1.01734 -1.							38	.0030	-1.48462	•	-1.47133
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							40	1.01734	-1,48557	1.01734	-1.48557

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MERIDIONAL AIRFOIL GEOMETRY. - STREAMLINE

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!	;	SURFA	SURFACE COORDINATES	ATES	1
>	T(M) PT	xs	۲S	άx	4
	.1.	28523 1.	73396 - 1	1.28523	1,73396
. 22544 1.	03019 2 -1.	28900 1.	72586 -1	•	1,73613
. 16565 1.58226 -	04041 3 -1.	-	72000 - 1	1.27118	1.73287
. 10587 1.50341 -	04995 4 -1.	-		1.21359	1.66845
.04608 1.	5 -1	- '		-1, 14963	1.59457
.98629 1.33945 -	06707 6 -1	. 12586 1.	48844 -1	1.08587,	1 51838
92651 1.25427 -	07463 7 -1	.1 6885 1.		1 02231	1.43983
.86672 1.16699 -	08148 8 -1	-	32002	-0.95896	1.35888
. 80693 1.07772 -	08760 9	95717 1		-0.89584	1,27553
.73519 0.96828 -	.0- 01 7920	90045 1		-0.83299	1,18983
.66345 0.85685 -	09923 11	-	.05352 -0	-0.77042	1.10192
.59170 0.74429	10338 12	ò	94270	-0.69578	0.99385
.51996 0.63172	10643 13,	-0.70524 0.	83012	-0.62165	0.88359
.44821 0.52035	10844 14	Ö	71654	-0.54809	0.77203
.37647 0.41118	•	o	60304	-0.47513	0.66039
.30473 0.30497	10960 16	Ö	49081	0.40275	0.54989
. 23298 0.20214 -	10893 17			-0.33091	0.44151
. 16124 0. 10274	₩.	-0.34991 0.	0.27397 -0	-0.25954	0.33598
0.00633	10557 19		•	-0.18856	0.23367
-0.08780 -	10301 20 -0			5,11787	0.13455
.05399 -0.18041 -	21	13164		-0.04735	0.03910
.12574 -0.27209 -	09639 22	O	11921	0.02307	
. 19748 -0.	09239 23 0.	01458	21112	0.09341	-0 14969
. 26923 -0.45337 -	08800 24 0.	08784), 16364	-0.24231
.34097 -0.54298	08325 25 0.	16126		0.23371	-0.33440
.41272 -0.63!86 -	07818 26 0.	23483 -0.	43081	0.30363	-0.42594
.48446 -0.	07282 27 0.	30853 -0.	56906	0.37341	-0.51690
-0.80727	06722 28 0.	38235 -0.	55648	0.44308	-0.60725
.62/95 -0.8936/	0614.2 29 0.	45628 -0.	74303	0.51264	0.69692
. 69969 -0. 97906	05546 30 0.	53029 -0.		0.58212	-0.78587
.77144 -1.06329	04938 31 0.	o ·	91336		-0.87399
.84318 -1,14616	04322 32 0.	ė.			-0.96116
.91492 -1.22737	03702 33 0.	75270 -1.	07938 C	0.79017	-1.04721
0.98667 -1.30666 -47	34	82691 -1.	16038 C	0.85945	-1.13193
1.04645 -1.37111 -46	Ö	90112 -1.	23971 0	0.92873	-1.21504
•	Ö	97530 -1.	31708 C	0.99803	-1.29624
	37 1 (03708 -1.	37992	1.05583	-1.36231
	-	09143 -1.	43393 1	1, 10675	-1.41923
	-	.1- 01860	43695	1, 10950	-1.42622
,	40	10624 - 1.	43401	1.10624	-1 43401
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MERIDIONAL AIRFOIL GEOMETRY - STREAMLINE 5

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THE DESIGNATION OF THE PROPERTY OF THE PROPERT

1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	λb	1.68911	1 69152	1.688-11	1.62370	1.54978	1.47371	1.39557	1.31544	1.23338	1.14952	1.06397	0.95938	0.85323	0.74654	0.64081	0.53743	0.43727	0.34063	0.24729	0.15674	0.06840	٠.			0.27292			-0.52212		٠.	-0.76610	-0.84605	-0.92515	-1.00326	-1.08020	-1,15530	-1.21768	-1.27121	-1.27810	-1.28622
DINATES	ΑX	- 1.36095	-1.35296	-1.34667	-1.28501	-1.21671	-1.14863	-1.08076	-1.01314	-0.94580	-0.87878	-0.81207	-0.73250	-0.65351	-0.57520	-0.49765	-0.42083	-0.34465	-0.26897	-0.19364	-0.11856		0.03113	0.10580	0.18034	0.25472	0.32895	0.40304	0.47701	0.55086	0.62462	0.69829	0.77190	0.84546	0.91900	0.99252	1.06607	1.12740	1, 18133	1,18453	1.18173
SURFACE COORDINATES	۸۶	1.68911	1.68182	1.67491	1.60317	1.52205	1,43945	1.35537	1.26987	1.18304	1.09496	1.00572	0.89734	0.78787	0.67818	•	0.46327	0.36054	0.26182	0.16711	0.07599	-0.01210	-0.03776	-0.18159	•	-0.34550	-0.42597	-0.50552	-0.58421	-0.66205	-0.73905	-0.81519	-0.89041	-0.96464	-1.03775	- 1, 10959	-1.18002	-1.23753	-1.28716	-1.28974	-1.28622
1 1 1 1 1 1 1 1 1 1	×S	- 1.36095	-1.36462	-1.36258	-1.30975	- 1,25092	-1.19187	-1.13261	-1.07309	-1.01329	-0.95319	-0.89276	-0.81977		-0.67195	-0.59694	-0.52120	-0.44482	-0.36794	-0.29070	-0.21322	-0.13557	-0.05779	0.02009	0.03811	0.17629	0.25462	0.33309		0.49040	0.56920	•	0.72704	0.80604	0.88507	0.96410	1.04312	1.10892	1.16672	1.17371	1,18173
	PT	-	8	ო	4	ល	9	7	€	6	ţ	=	12	Ļ	7	15	16	11	2	49	20	21	22	23	24	25	56	27	28	29	9	31	35	33	34	32	36	37	38	33	40
	1 (M)	0.01959	0.03215		•	•		0.08420	0.09227	٠,	0.10709	0.11342	0.11847							0. 122 18	٣,	0.11569			0.10170	0.09611			0.07712	0.07021		0.05580	•	0.04088		0.02712	0.02089				
	o) ¥•	-49.624	-50 313	•		-52.208	•	-53,282	-53.752	•	-54.580	-54.813	-54.757	•	-53.541	-52.548	-51.468			-48.788	-48.213	-47.802	-47.492		-46.956	-46.702	-46.450	•	•	•	-45.323	•	-44.526	-44.024	-43.457	-42.945	-42.410				
INE DATA	>	1.68911	1.61343	1,53591	1.45658	1.37547	1.29265	1.20821	1.12224	1.03485	0.92835		0.71236			٠		٠.	0.11636	0.02815	٠.	•	,	•	•	-0.47257		-0.63305	•	-0.79064	-0.86823	-0.94489	-1.02050	-1.09489	-1,16791	-1.22761	-1.28622				
MEANLIN	×	-1.36095	Ť.	-1.23382		-1,10668	-1.04312	-0.97955	-0.91598	-0.85242	-0.77614	-0.69985	-0.62357	-0.54729	-0.47101	-0.39473	-0.31845	-0.24217	-0.16589	-0.08961	-0.01333	0.06295	0.13923	0.21551	0.29179	0.36807	0.44435	0.52063	0.59691			0.82575	0.90203	0.97831	1.05459	1.11816	1.18173				
	PCT X		0.02500	0.05000		~	~	0.15000	0.17500	0.20000	0.23000	0.26000	0.29000	0.32000	0.35000	0.38000	0.41000	0.44000	0.47000	0.50000	0.53000	0.56000	0.59000	0.62000	0.65000	0.68000	~	0.74000	0.77000	0.80000	$\mathbf{\omega}$	00	0.89000	0.92000	0.95000	0.97500	1.00000				
:	P.	-	N	ო	₹	ស	9	7	∞	6	9	=	12	1 3	7	1 5	16	17	1 8	1 9	20	21	22	23	24	22	56	27	28	53	ဓ္ဌ	3	32	33	34	32	36				

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Ç MERIDIONAL AIRFOIL GEOMETRY - STREAMLINE

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ÞΙ	PCT X	×	>	₩.	T (M)	pT	×S	۸۶	ďX	46
-	°.	•	1.62617	-48.221	0.01963	-	-1.43240	1,62617	-1.43240	1.62617
8	٠	•	1.55039	-48.761	0.03479	7	-1.43593	1.61872	-1.42445	1.62882
ო	0.05000	-1.29829	1.47319		0.04922	က	-1.43377	1.61184	-1.41800	1.62590
4	٠.		1.39460		•	~	-1.37842	1.53893	-1.35226	1.56186
ហ	┺.	-1.16417	1.31469		0.07560	ស	-1.31694	1,45714	-1.27963	1.48925
9	Ξ.	-1.09711	1.23356			9	-1.25521	1.37432	-1.20726	1.41489
7	Τ.		1, 15133		٦.	7	-1.19322	1.29051	-1,13512	1.33888
œ	•	-0.96300	1.06814			80	-1.13095	1,20579	-1.06328	1.26133
6	"	-0.89594	0.98415	-51.508		6	-1.06834	1.12030	-0.99177	1.18235
9		-0.81547	0.88261		. 12	5	-1.00537	1.03416	-0.92063	1.10212
Ξ	0.26000	-0.73500	0.78076	-51,656	0.13549	-	-0.94201	0.94751	-0.84987	1.02079
4		-0.65453	0.67952	-51.327	0.14211	12	-0.86542	0.84312	-0.76552	0.92209
ლ	е.	LD.	0.58018	-50.586	0.14718	<u></u>	-0.78813	0.73874	-0.68187	0.82279
4	r;	-0.49359	0.48402	-49.519	٦.	4	-0.71000	0.63512	-0.59906	•
15	က	-0.41312	0.39175	-48.275	Τ.	5		0.53345	-0.51721	
16	۳.	-0.33265	0.30347	-47.044	0.15370	16	-0.55093	0.43508	-0.43626	
17		-0.25218	0.21865	-46.005	┺.	17		0.34087		0 44263
₩	•	-0.17172	0.13655	-45.168	0.15173	1 8	-0.38890	0.25110	-0.27641	
6	'n.	-0.09125	0.05659	-44.490	٠.	6		0.16542	-0.19705	
20	ĸ.	-0.01078	•	-43.942	0.14572	50	-0.22552	0.08307	-0.11791	0.19004
2		0.06369	•		0.14141	21	-0.14352	0.00338	-0.03897	0.10981
22		0.15016	•		0. 13632	22	-0.06134	-0.07414		•
23	•	0.23063			0.13052	23		-0.14990		-0.04733
5	•	0.31110			٣.	24		-0.22421		-0.12472
25		0.39157	-0.39669	-42.146	0.11705	25	0.18630	-0.29728	0.27496	
56		0.47204	•	-41.822	0.10951	26	0.26922	-0.36921	0.35299	-0.27768
27	0.74000	0.55251	•	-41.488		27	0.35230	-0.4400B		-0.35329
28		0.63298	•	-41.143	•	58			0.50855	
58		0.71345	٠	-40.792		29		-0.57870	•	-0.50268
ဓ္ဓ	∞.	0.79392		-40.435	0.07527	30	0.60236	-0.64647	٠.	-0.57638
31		0.87439	_:	-40.076	0.06600	31	0.68591	-0.71321	0.74099	-0.64938
35		٠	_•	-39.720	0.05653	32	0.76951	-0.77895	0.81333	-0.72165
33	o.	.0353	٠.	-39.370	0.04692	33	0.85314		0.89563	-0.79318
34		. 1157	-1.01777	6		34	0.93679	9074	0.97292	-0.86397
35		. 182	-1.07185	-38.738	6	35	1.02044	-0.97029	1.05021	-0.93401
36	1.00000	1.24991	-1.12537	-38.451	0.02105	36	1.10407	-1.03224	1.12752	-1.00331
						37	1.17373	-1.08321	1, 19197	-1.06048
						38	1.23482	-1, 12746	1,24854	- 1,11020
						33	1.24210	-1,12951	1,25219	-1.11692
						40	1.24991	-1,12537	1.24991	-1,12537

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MERIDIONAL AIRFOIL GEOMETRY - STREAMLINE

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THE REPORT OF THE STREET OF THE STREET OF THE STREET OF THE STREET STREET STREET OF THE STREET STREE

	dλ	1.54405	1.54688	-	1.48113	1.41021	1.33787	1.26420	1 18931	1,11336	<u>-</u>	Ö	0.86742	ò		ó	Ö	ö	ö				0.06259		ġ.	o O	φ̈	o-	Ŷ	ġ.	o O		ġ	o,	o o	ġ.	O	o O	o O	ġ.	-0.98206
RDINATES	ά×	-1.50326	-1,49551	-1.48906	-1.41906	-1.34207	-1.26535	- 1, 18890	-1.11277	- 1.03704	-0.96176	-0.88703	-0.79815	-0.71022	-0.62330	-0.53737	-0.45236	.0.36809	-0.28440	-0.20107	-0, 11806	-0.03538	0.04699	0.12910	0.21098	0.29267	0.37418		0.53681					0.94153	1.02232	1.10313	1,18397	1.25137	1.31037	₹	1.31294
SURFACE COORDINATES	۲S	1.54405	1,53661	1.52989	1,45563	1.37307	1,28985	1.20600	1, 12163	1.03688	0.95197	0.86724	0.76639	0.66720	0.57045		0.38704	0.30125	•	0.14136	0.06632	-0.00609	-0.07620	-0.14422	-0.21035	•			-0.45936	-0.51850	-0.57662		-0.68992			-0.85259		.0.94821	-0.98557	-0.98693	-0.98206
	XS	-1.50326	-1.50659	-1.50437	-1.44665	-1.38283	-1.31875	-1.25438	-1.18970	-1.12462	-1,05909	-0.99301	-0.91297	-0.83187	-0.74983	-0.66678	-0.58282	-0.49811	-0.41284	-0.32720	-0.24123	-0.15494	-0.06834	0.01852	0.10562	0.19290	0.28036	0.36795	0.45568	0.54352	0.63147	0.71952	•		0.98400	1.07216	1.16030	1.23371	1.29793	1.30544	1.31294
:	þŢ	-	8	ო	4	ស	9	7	∞	6	5	=	12	ნ	<u>~</u>	1 5	9	1	⊕	6	2	21	22	23	24	25	56	27	28	59	9	34	35	33	34	32	36	37	38	33	40
	T(M)	0.01923	0.03757	0.05514		0.08761	0.10245	0.11628	0.12901	0.14060	-		0.17208	0.17891		-	0.18885	-	•				0.16894		•	•	0.13519			0.10301	0.09137	•		•	•	0.03169	0.02116				
	M·N	-46.856	-47.267	-47.661	-48.032	-48.371	-48.659	-48.874	-48.975	-48.923	-48.642	-48.111	-47.333	-46.330	-45.178	٠	-42,855	-41.898	-41.089	-40.374	-39.727		-38.584		-37.645		-36.879	-36.543		-35.877		'n.	•	-34,438		•	-33.604				
INE DATA	>	1.54405	1.46838	1.39164	1.31386	1,23510	1,15547	1.07512	0.99431	0.91343	-	0.72175	0.62877	0.53864	0.45187	0.36861	0.28870	0.21165	0.13694	0.06421	-0.00680	-0.07626	-0.14432	-0.21112	-0.27680	-0.34149	-0.40529		-0.53053	•	-0.65273	-0.71263	-0.77171	-0.83001	-0.88759	-0.93506	-0.98206				
MEANLIN	×	-1.50326	-1.43286	-1,36245	-1.29205	-1.22164	-1,15124		-1.01043	-0.94002	-0.85553	-0.77105	-0.68656	-0.60208	-0.51759	-0.43310	-0.34862	-0.26413	-0.17965	-0.09516	-0.01067	٠.					0.49624				•		•	1.08765	1.17213	1.24254	1.31294				
	PCT X	· o	0.02500	•	0.07500	0. 10000	₹.		0.17500		7		0.29000				4										0.71000					œ				•	1.00000				
:	ΡŢ	-	ď	ო	4	'n	9	7	30	6	₽	Ξ	12	1 3	7	15	46	11	2	19	20	21	22	23	24	25	56	27	28	53	ဓ္က	3	32	33	34	32	36				

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MERIDIONAL AIRFOIL GEOMETRY - STREAMLINE

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-1.57268 1.44253 -45
-1.49905 1.36700 -45
-1.42542 1.29073 -46.
-1.35180 1.21380 -46.
-1.27817 1.13635
20454 1,03859 -46.
-1.05228 0.90330
-0.98365 0.82667
-0.89530 0.73662 -4
o.
-0.71859 0.
-0.63023 0.48554
.54188 0.40877 -40
.45353 0.33509 -39
.36517 0.26410 -38
.27682 0.19536
. 18846 0.12847
-0.10011 0.06322 -
-0.01175 -0.00048
0.07660 -0.06266 -
0.16496 -0.12336 -34.
0.25331 -0.18263 -
0.34167 -0.24055 -
0.43002 -0.29721 -3
.51837
0.408/3 -0.46/50 -
0.78344 -0,51311 -
0.87179 -0.
0.96015 -0.61548 -
1.04850 -0.66540 -
1,13686 -0,71454 -2
1.22521 -0.76294 -
1.29884 -0.80276 -
1.37247 -0.84210 -

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MERIDIONAL ÁIRFOIL GEOMETRY - STREAMLINE 9

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	:	MEANLIN	INE DATA		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	:	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	SURFACE COORDINATES	DINATES	
ÞΙ	PCT X	×	>	80 · M	1(M)	14	sx	8>	×	dλ
~	o.	-1.62751	1.30702	-44.404	0.01815	-	-1.62751	1.30702	-1.62751	1,30702
8	0.02500	-1.55076	1.23175	-44.482	0.04013	~	-1.63038	1.29980	-1.62033	1.31004
ო	•	-1.47402	1.15632	-44.519	0.06166	က	-1.62806	1.29356	-1.61405	1.30786
*	٦.	-1.39728	1.08090	-44.467	0.08259	*	-1.56482	1.21744	-1.53670	1.24607
ស	0. 10000	-1.32053	1.00578	-44.283	0.10233	ß	-1.49564	1.13434	-1.45240	1.17830
9		-	0.93134	-43.943	0. 12222	ဖ	-1.42620	1.05143	- 1.36835	1.11037
7		-1.16704		-43,430	0.14061	7	-1.35643	0.96897	-1.28463	1.04258
&	0.17500	- 1.09030	0.78617	-42.749	0.15787	œ	-1,28619	0.88734	-1.20138	0.97534
6		-1.01356	0.71623	-41,911	0.17390	6	-1.21538	0.80694	-1.11871	0.90905
5		-0.92146		-40.727	0. 19136	\$	-1.14388	0.72920	-1.03672	0.84413
Ξ		-0.82937	•	-39.405	0.20679	=	-1.07163		-0.95548	0.78094
12			0.48388	-38.057	0.22012	12	-0.98389	0.56272	-0.85904	0.70773
13		-0.64518	₹.	-36.798	0.23131	,	-0.89500	0.47785	-0.76374	0.63763
4		-0.55309	0.34597	-35.662	0.24037	7	-0.80512		-0.66943	0.57054
Ť.	0.38000	-0.46100	ď	-34.654	0.24726	ŧ	-0.71446			
1	0.41000		0.21855	-33.758	0.25193	16	-0.62316	0.24833	-0.48302	0.44362
17	•	-0.27681	0.15794	-32.949	0.25434	11	-0.53130	0.17943	0.39070	
⊕		-0.18472	0.09912	-32.190	0.25445	18	-0.43890	0.11382	-0.29891	0.32327
19		-0.09263	0.04198	-31.446	0.25228	5	-0.34598	0.05123	-0.20765	0.26466
50			-0.01352	-30.698	0.24800	20	-0.25250	-0.00855	-0.11694	0.20679
2		٠.	-0.06737	-29.939		21	-0.15843	-0.06563	-0.02682	0.14959
22			-0.11961	-29.188		22	-0.06384	-0.12014	0.06277	0.09310
23	•		-0.17029	-28.467	0.22431	23	0.03122	-0.17214	0.15190	0.03739
24		0.36784	-0.21951		0.21331	24	0.12663	-0.22169	0.24067	-0.01753
25			-0.26735	-27.127	0.20101	52	0.22229	-0.26888	0.32920	-0.07170
56			-0.31389	-26.502	0.18753	26	0.31813	-0.31387	0.41755	-0.12514
27			-0.35921	-25,904	0.17302	27	0.41411	-0.35680	0.50576	-0.17790
28		•		-25.328	•	28	0.51018		•	-0.22998
59				-24.773	0.14135	29	0.60632		0.68191	
30	0.83000	•		-24.236	0.,12442	30	0.70250	-0.47458	0.76992	
31		٦,	-0.52933		0.10692	31	•			
35		1.10458		•	0.08898	35	•		0.94593	-0.43165
33	•	1.19667	•	-22.737	0.07069	33	0.99099	-0.57828	1.03399	-0.48038
34		83	•	ä	0.05218	34	1.08704		1.12212	
32	٠	1.36551		ᅷ.	•	32	1.18301		1.21034	
36	1.00000	1.44226	-0 70817	-21.506	0.02111	36	1.27888		1,29866	.6223
						37	1.35868		1.37235	
						38	1.42824		1.43672	
						33	1.43589		1.44207	
						40	1.44226	-0.70817	1.44226	-0.70817

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Y B+M T(M) PT XS YS XP 12766 -42.756 0.02070 1 -163023 1 112706 -1.62023 1 12706 -1.62023 1 12706 -1.62023 1 12706 -1.62023 1 11872 -1.62227 1 1.62023 1 11872 -1.62227 1 1.62023 1 1.11872 -1.62227 1 1.62023 1 1.11872 -1.62227 1 1.62023 1 1.62023 1 1.62023 1 1.62023 1 1.62023 1 1.62023 1 1.62023 1 1.62023 1 1.62023 1 1.62023 1 1.62023 1 1.62023 1 1.62023 1 1.62023 1 1.62023 1 1.62023 1 1.62023 1 1.62023 1 1.6603 1 1.62023 1 1.6603 1	!	- MEANLINE DATA					SURFACE COURDINATES		
-42.850 0.02070 1 -163033 1 11870 -1 63033 1 11870 -1 63033 1 11870 -1 61527 1 11872 -1 63034 -1 11870 -1 61522 1 11870 -1 61522 -1 61534 -			X	T(M)	PT	xs	s,	×	ď×
-42.795 0.04299 2 -163338 1.11872 -165227 1.42.66 -42.668 0.08694 4 -1.65654 1.1177 -161503 1.42.66 -42.668 0.08694 4 -1.65654 1.03777 -1.53640 1.53640 -41.849 0.10820 5 -1.49375 0.95529 -1.44860 1.36541 -39.932 0.14837 7 -1.34911 0.71700 -1.19690 0.17700 -37.531 0.14828 7 -1.20703 0.64087 -1.10699 0.01710 -37.531 0.14829 1 -1.20703 0.64087 -1.10699 0.01710 -37.532 0.14839 0.11730 0.64087 -1.10699 0.01710 -37.531 0.14829 0.01710 0.74771 0.74771 0.01740 -30.747 0.20248 0.1173 0.022674 0.11069 0.022674 -31.248 0.20248 0.77530 0.74771 0.022740 0.022740 -30.179 0.26970 1.105183 0.024053 0.022740 0.02202<	<u>-</u>	ဖွ	-42.850	•	-	-1.63033	1.12706		1.12706
-42.568 0.08514 3 -1.63054 1.11170 -1.61503 1.1 -42.568 0.08514 3 -1.63054 1.0377 -1.53640 1.1 -41.849 0.10820 5 -1.49375 0.95629 -1.44960 1.1 -41.849 0.10820 5 -1.49375 0.95629 -1.44960 1.1 -39.992 0.14833 7 -1.34911 0.39733 -1.35640 1.1 -39.992 0.14835 7 -1.34911 0.39539 -1.3669 0.1 -39.778 0.16691 8 -1.27596 0.71700 -1.19142 0.1 -30.738 0.22081 11 -1.05183 0.40715 -0.93957 0.1 -31.243 0.22081 11 -1.05183 0.41677 -0.84059 0.1 -32.345 0.22081 11 -1.05183 0.41677 -0.84059 0.1 -30.179 0.26074 14 -0.49222 0.34063 0.74240 0.1 -29.129 0.22074 14 -0.49232 0.07311 -0.35674 0.1 -29.129 0.22054 17 -0.49232 0.07311 -0.35674 0.1 -20.02074 0.22021 18 -0.30077 -0.04189 0.16812 0.1 -20.02074 0.22021 18 -0.30077 -0.04189 0.16812 0.1 -20.02074 0.22021 18 -0.30077 -0.04189 0.10793 0.1 -20.02074 0.22021 18 -0.30077 -0.04189 0.10793 0.1 -20.02074 0.22021 0.00735 -0.18496 0.11073 0.1 -20.02021 0.00735 -0.18496 0.11073 0.1 -20.02021 0.00735 -0.00735 0.03857 -0.00739 0.1 -20.02021 0.00735 0.009109 -0.26572 0.07481 0.1 -20.02021 0.00033 0.009109 -0.26572 0.00739 0.1 -20.0203 0.00033 0.00033 0.00030 0.00030 0.1000 0.1000 0.1 -20.0203 0.0003 0.00030 0.00030 0.1000 0.1000 0.1 -20.0203 0.0003 0.00030 0.00030 0.1000 0.1000 0.1 -20.0203 0.0000 0.1200 0.00000 0.10	- (-42.795		~	-1.63338	1.11872	-1.62227	1.13073
-41. 389 0.10894	.4/16/ 0.98023 39334 0.90344		-42.668	0.06514	m •	<u>.</u> .	1.11170	. 1.61503	1.12843
-41.050 0.12873 6 -1.42164 0.87533 -1.36304 0.10691 0.16835 7 -1.34911 0.79536 -1.27692 0.14835 7 -1.34911 0.79536 -1.27692 0.14835 7 -1.34911 0.79536 -1.27692 0.14835 9 -1.20703 0.64037 1.10669 0.10603 0.20349 10 -1.12730 0.56749 -1.02276 0.10603 0.22081 11 -1.05183 0.40715 -0.93957 0.34059 0.22081 11 -1.05183 0.407715 -0.93957 0.34059 0.22081 11 -1.05183 0.24063 0.34063 0.24053 13 -0.86822 0.34063 -0.74240 0.22076 0.26074 14 -0.77530 0.26840 0.26443 0.26074 15 -0.77530 0.26840 0.26443 0.28021 15 -0.68167 0.19983 0.26421 0.26528 0.22631 0.28054 17 -0.49532 0.07311 0.26528 0.22631 0.28054 17 -0.49560 0.01480 0.04493 0.22631 0.28054 17 -0.49660 0.01480 0.04493 0.22703 0.22703 0.27733 0.22703 0.02773 0.02673 0.			-41.849	٠,	rus		1.03/// 0.95639	1.33640	1.0083.
-39.992					, φ	-1.42164	0.87533	: _:	0.93955
778 0.16691 8 -1.27596 0.71700 -1.19142 0.0 531 0.18428 9 -1.20203 0.64087 -1.10669 0.0 534 0.22084 11 -1.20203 0.64087 -1.10669 0.0 738 0.22084 11 -1.05183 0.43715 -0.93957 0.0 504 0.23618 12 -0.96042 0.41677 -0.94059 0.0 345 0.24953 13 -0.96042 0.41677 -0.94059 0.0 345 0.24953 13 -0.96042 0.41677 -0.94059 0.0 345 0.26974 14 -0.76813 0.74240 0.0 0.0 345 0.26974 17 -0.68177 0.04918 0.054817 0.054817 0.0 0.0 348 0.28054 14 -0.68135 0.04188 0.054817 0.05178 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0			-39.992		7	-1.34911	0.79536	-	0.87596
531 0.18428 9 -1.20703 0.64087 -1.10669 0 738 0.20349 10 -1.12730 0.54715 -1.02276 0 738 0.22081 12 -0.96042 0.41677 -0.84059 0 554 0.23618 12 -0.96042 0.41677 -0.84059 0 345 0.24953 13 -0.86822 0.34063 -0.74340 0 179 0.28054 17 -0.49232 0.13477 -0.45211 0 178 0.28054 17 -0.49232 0.07311 -0.45211 0 078 0.28054 17 -0.49232 0.07311 -0.45211 0 078 0.28054 17 -0.49232 0.07311 -0.16812 0 078 0.28054 10 0.03114 -0.36014 0 0 078 0.28057 0.04018 0.04781 0 0 0 080 0.2720 22 </td <td>57503</td> <td></td> <td>38</td> <td></td> <td>60</td> <td>-1.27596</td> <td>0.71700</td> <td>•</td> <td>0.81409</td>	57503		38		6 0	-1.27596	0.71700	•	0.81409
0.20349 10 -1.12730 0.56749 -1.02276 0.022081 11 -1.05183 0.43715 -0.93957 0.22081 11 -1.05183 0.43715 -0.93957 0.224953 13 -0.966822 0.34063 -0.74240 0.22697 14 -0.77530 0.26840 -0.64493 0.26970 15 -0.686822 0.34063 -0.74240 0.226970 15 -0.68167 0.19983 -0.54817 0.226970 15 -0.69167 0.19983 -0.54817 0.226970 15 -0.058735 0.07311 -0.35674 0.028 0.228130 19 -0.39660 0.01480 -0.26208 0.028130 19 -0.39660 0.01480 -0.26208 0.028130 19 -0.30017 -0.04018 -0.26208 0.27727 21 -0.10544 -0.14000 0.01703 0.225480 22 -0.00735 -0.18496 0.11073 0.225480 23 0.09109 -0.22582 0.20318 0.014020 0.01703 0.225480 23 0.09109 -0.22582 0.20318 0.02857 0.23837 -0.225480 23 0.28867 0.38759 0.26575 0.23837 -0.225480 0.38759 0.28879 0.39542 0.56801 -0.225480 0.19038 27 0.48681 0.36633 0.56801 -0.225480 0.16268 0.38759 0.28879 0.39542 0.56891 0.20318 0.16296 0.14429 30 0.788389 0.39542 0.05928 0.058599 0.39549 0.39542 0.05903 34 1.18008 0.55497 1.20747 0.05903 34 1.18008 0.55497 1.20747 0.05903 34 1.18008 0.55497 1.20747 0.05903 34 1.18008 0.55491 1.27862 0.55401 1.1580 0.00137 0.05903 34 1.18008 0.55400 1.55127 0.55317 0.05109 35 1.527996 0.55720 1.55127 0.05720 0.57200 0.57201 0.00113 0.00112 0.00112 0.00113 0.001	. 99570		37.		6	••	•	-1.10669	
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MERIDIONAL AIRFOIL GEOMETRY - STREAMLINE 11

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MERIDIONAL AIRFOIL GEOMETRY - STREAMLINE 12

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Α×	0.79605	ó	0.8001	ö	79 0.69747	ċ														54 0.07984				Ġ.	•	Ċ	o O	ó.		O	09 -0.15535	0		•		7 -0.		55 -0.20443	
X	-1.64701	-1.63409	-1.6215	-1.54677	-1.45779	-1.36922	-1.28113	- 1, 19350	- 1.1067	-1.02055	-0.9351	-0.83359		-0.63339	-0.5343	-0.435R6	-0.33793	-0.24057	-0.14381	-0.04754	0.0483			0.33437			•			0.90366	0.99909	1.09500	1, 19146	1.28854	1.38632	1.4849	1.56798	1.6305	
۸S	0.79605	0.78153	٠	0.70770	0.63454	0.56318	0.49377	0.42650	•	•	٠:		0.10801	0.04882	-0.00609	-0.05697	-0.10401		-	-0.22273										-0.38028	-0.37590		-0.35570	-0 33988	•	-0.29614	-0.27275	-0.25345	
sx	-1.64701	-1.65114	-1.64561	-1.58213	-1.50599	-1.42944	-1.35241	-1.27482	-1.19658	-1.11763	-1.03794	-0.94133	-0.84371		-0.64614		-0.44627			-0.14222	-0.03995	٠.		0.26844					0.78493		0.99073	1.09297	1.19464	1.29571	1.39607	1.49557	1.57768	1.63849	
ΡŢ	-	~	က	~	ស	9	7	80	6	5	Ξ	7	13.	4	ŧ,	16	17	₩	1 9	20	51	22	23	24	22	56	27	28	53	ဓ္ဌ	31	32	33	34	35	36	37	338	
T(84)	0.03474	0.05714	0.07927	0. 10101	0.12226	0.14288	0.16272	0.18169	0.19973	0.22001	•		•	0.28419	0.29556	٠,	e.	0.31704		0.31995	•			0.29738		0.27285			. 52		0.17618	0.15115	0.12433	0.09540	0.06956	0.04286			
B·N	•	-38.229	•	•		-34.642		•							-21.504	-20.126	-18.745	•	- 16.032	-14.718	-13.429	- 12.149	•			•	•		٠	-0.584	1.035	•	4.498	6.380	8.022	69			
>	0.79605	0.73014	0.66601	C. 60373	0.54344	0.48528	ς.	ς.	0.32507	0.26750	0.21377	0.16379	0.11728	0.07392	0.03349			-0.07144		-0 12841				-0.21374					•	•	-0.26763	-0.26439	-0.25816	•	-0.23831	-0.22545			
×	-1.64701	.5644	1.48189	-1.39933		-1.23421	-1,15165	-1.06909	-0.98653	-0.88746		-0.68931	-0.59024	-0.49117	-0.39210	-0.29303	-0.19395	-0.09488	0.00419	•	0.20233	0.30141	0.40048	0.49955	0.59862	0.69769	0.79677	Φ.	ο.	1.09398	1,19305	1.29213	1.39120	1.49027	3	553			
PCT X	o.	•	•	o.	٣.	٣,	۲.		7	•	•	•	•		0.38000	٩.	•	•			•	•		0.65000	•	۲.			•		0.86000		0.92000	0.95000	0.97500	1 00000			
ΡŢ	_	8	က	4	ស	9	7	ထ	ۍ.	0	Ξ	72	.	4	ا 5	16	11	8	49	2	21	22	23	24	25	56	27	28	59	30	3.	32	23	34	33	36			

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MERIDIONAL AIRFOIL GEOMETRY - STREAMLINE 13

ADT HOUSE THE TOWN OF THE POSSESSE SECRETARIES CONTINUES CONTINUES SECRETARIES SECRETARIES FOR FOR HOUSE REPORTED FOR THE POSSESSES OF THE POS

•	; ; ; ; ; ;	MEANLINE	INE UNIN		 	:	* * * * * * * * * * * * * * * * * * *	SURFACE COURDINALES	UINAIES	: : : : :
ΡŢ	PCT X	×	>	B • N	T(M)	μ	XS	۲S	άx	ΥP
	o	-1.68351	0.69765	-33.040	0.05298	-	-1.68351		-1,68351	
	0.02500	-1.59952	0.64345	-32.621	0.07293	7	-1.68748	0.67516	-1.66494	0.71037
	0.05000	-1.51553		-32,148	0.09291	ო	-1.67723	0.65887	-1.64558	0.70774
	0.07500	-1,43154		-31,615	0.11279	4	-1.61918	0.61274	-1.57986	0.67417
ß	0.10000	-1.34755		-31.026	0.13240	ស	-1.54025	0.55084	-1.49081	0.62951
9	0.12500	÷	•	-30.374		9	-1.46110	0.48989		0.58594
7	Ξ.	-1.17957	0.38839	-29.645	0.17028	7	-1.38167	0.43007	-1.31343	0.54353
80	0.17500	- 1,09558	•	-28.806	0.18834	6 0	-1.30188	0.37152	-1.22523	0.50231
6	- 1	-1.01158	•	-27.832		თ	-1.22168	0.31439	-1.13745	0.46239
•	0.23000	-0.91079	•	-26.489	0.22546	₽	-1,14095	0.25886		0.42390
=	0.26000			-24.989	0.24397	Ξ	- 1.05960		-0.96357	0.38704
12		-0.70922	0.15042	-23.419	0.26104	12	-0.96108		-0.86051	0.34524
13		-0.60843		-21.850	0.27658	<u>€,</u>	-0.86154	0.08517	-0.75847	0.30630
4			•	-20.313	0.29050	4	-0.76109	0.03065	-0.65734	0.27019
15		-0.40685		- 18,830	0.30272	5		-0.01996	-0.55696	0 23675
16	0.41000	-0.30606		-17.416		16	-0.55806	-0.06667	-0.45722	0.20576
17				- 16.062	0.32170	17			-0.35800	0.17698
18		-0.10448	-0.05733	-14.747	•	€	-0.35292	-0.14866	-0.25920	0.15014
19		-0.00369		-13.454	•	6	-0.24977	-0.18414	-0.16077	0.12501
20				- 12. 172		20	•	-0.21607	-0.06270	0.10141
21	0.56000			- 10.906	•	2.		-0.24450	0.03503	0.07920
22	0.59000		-0.14444	-9.671		22	C.06176	-0.26941	0.13244	0.05826
23		0.39946		-8.433	0.32897	23		-0.29080	0.22961	0.03851
24	0.65000	0.50025		•	0.32251	24	0.27068	-0.30871	0.32667	0.01983
25		0.60104		-5.670	٠.	25	0.37534	-0.32321	0.42359	0.00221
26		0.70183	-0.19418	-4.007		56	0.48026	-0.33430	0.52025	-0.01428
27		0.80262		-2.110		27		-0.34182	0.61655	-0.02941
28		0.90341		•		28		-0.34548	0.71243	-0.04288
29	0.80000	1.00420		•		53		-0.34488	0.80797	-0.05431
30	0.83000	1.10499	-0.19341			ဓ္ဓ	0.90339	•	0.90343	-0.06337
31	0.86000	•		7.284	0.22099	31	1.00934		0.99906	-0.06974
32	0.89000	1.30657		9.987	0.19881	32	1,11489		1.09509	-0.07314
33	0.92000	1.40736		12.802	0.17474	33	1.21979	-0.29245	1.19177	-0.07324
34	0.95000	1.50815		15.737	0.14821	34	1.32381	-0.26545	1.28933	-0.06965
35		1.59214	-0.09596		0.12403	32	1.42672		1.38800	-0.06205
36	т.	1.67613	٠.	20.782	0.09882	36	1.52825	-0.19296	1.48805	-0.05030 -0.05030
						37	1.61157	-0.15485	1.57270	-0.03706
						38	1.64870	٠	1.61168	-0.02980
						33	1.67352	-0.11116	1.64895	-0.03517
						40	1.67613	-0.06617	1,67613	-0.06617

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STAGGER

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3. PLANE SECTION BLADE COORDINATES

M. Landerstein L. Francisco Control L. Charles

Figure 31 shows the stacked Phase I rotor plane sections. The following tabulation gives the coordinates for these sections. These sections are spaced one half inch apart, beginning at the tip height of 8.5 inches and progressing inward to 2.5 inches. These are the same section locations as given for the baseline rotor in Reference 1. Also included in the tabulation are coordinates for the section meanline, the meanline angle, and the section percent thickness at each point. Plane section chord, camber angle, and stagger angle are also given. These coordinates are intended to represent the blade under hot running conditions and do not include any corrections for blade untwist, meanline deformation, centrifugal growth or thermal growth.

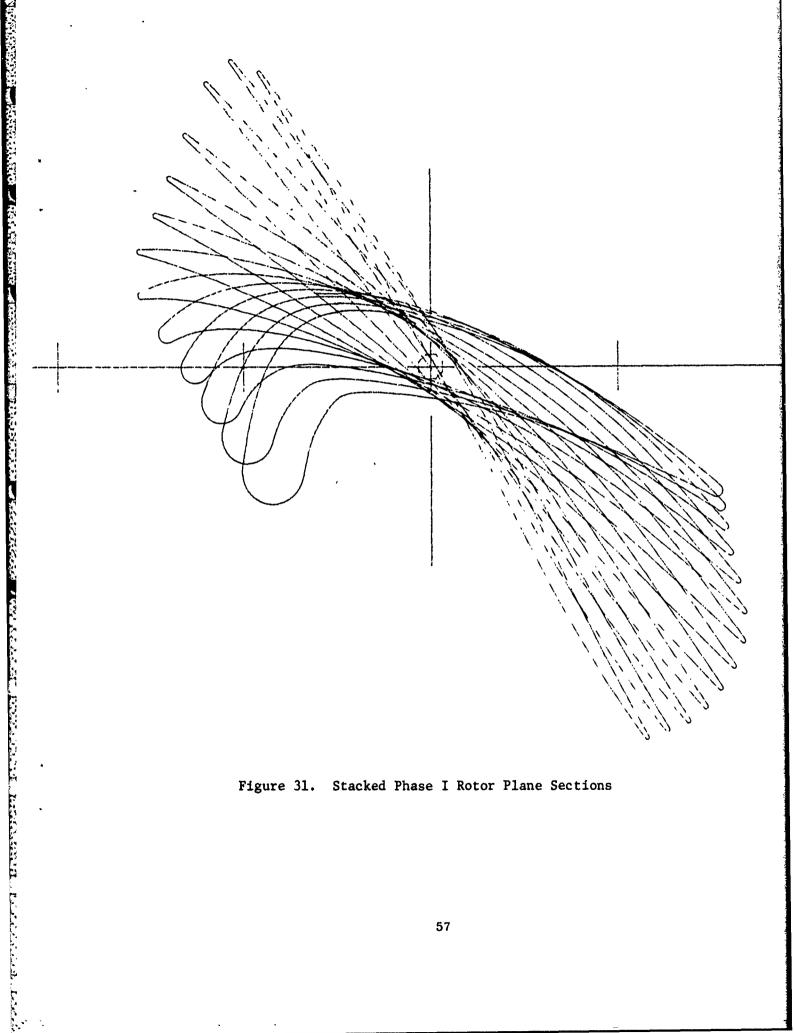


Figure 31. Stacked Phase I Rotor Plane Sections

WIND ARCOND AND AND THE CONTROL OF THE PARTY OF THE PARTY

SECTION AXIS GRIGIN AT MEANLINE COURDINATES WITH

58

ZETA*	56.212	•	57,386			•	•	•	•			62,559					
UPSILON	1.78981	1.71618	1.64069	1.56299	1.48309	1,40106	1.31691	1.23057	1.14203	1.03311	0.92177	0.80892	0.69565	0.58317	472	0.36424	258
ALPHA	-1.09072	-1.04171	-0.99270	-0.94369	-0.89469	-0.84568	-0.79667	-0.74767	-0.69866	-0.63985	-0.58104	-0.52223	-0.46342	-0.40462	-0.34581	-0.28700	-0.22819
1/0		0.00770	0.01036		5		0.01869	0.02024	0.02157	0.02291	0.02395	0.02473	025	0.02553	025	0.02551	0.02525
PCT AL	o.		0.0500			•	•	0.1750		0.2300		0.2900	0.3200		38	0.4100	0.4400
F.	-	N	၈	4	SO.	9	7	6 0	G)	0	=	72	ნ	4	<u>.</u>	16	17

MAR COMPANIENT AND PROPERTY AND PROPERTY OF THE PROPERTY OF TH

20	ETA. 0.	8.5000	AXIS	ZETA*	59.744	•	•		•	57.228	56.972	70.00	00.00g	15.04. 15.081	. 000 . SE	55,600			10	0	55.123	55.134	1.078	AXIS	UPSTEON			1.79119	1.78768	1.72415	. 60.18	1 49766	1 41764	1 33443	1 24917	1 15150	1.05338	0.94267	0.83033))))
2	¥C O	RHO	AT SECTION	UPSILON	0.15643	•	ö		-0.22776	-0.31967	-0.41055	-0.00063	-0.08004	-0.0/0/-	-0.8388	-0.93984	-1.02546	-1.11053	-1,19506	-1.27934		-1.41994	1.078	AT SECTION	LOWER A! PHA		•	-1.08315	•		-0.97630	-0.96331	10.02.02 10.02.02			10.66904	i c	> c	0000	1
1. ROTOR	620 R O.	SECTION AA	TES WITH ORIGIN	ALPHA	-0.16938	•		0.00202	0		0.18347	•	0.30	•	•	0.53632	•					. 8695	58.586	COORDINATES WITH ORIGIN	UPPER		<u>-</u>	.	٠	,	-,			~ •		- •			•	200
STAGE	N Z -7.03620	-	NE COORDINATES	1/0		٠.	-	•	•		0.02029				0.0100			0.01035		•	0.00631				AH PHA		-1.09072	•	•	•			- C. W. O		j c		-0.73423 -0.67786		0.00 0.00 0.00 0.00	. 5665
	SYSTEM ORIGIN	SECTION NO	MEANL I NE	PCT AL		•	•	•	•	•	0.6500	•	•	•	000	•					•	1.0000	3.7610	SURFACE	2,1	2	•	٠.			•	•	0.01490	•			0.02137	•	9 6	. 024
	COORD			F	18	9	50	21	22	53	24	n (9 I Q	, d	0 0	000	3.5	35	33		ා සි)- Q	-	-	N ·	n	4	in (1 0	~ 0	0 0	ָה מ	2 :	- 0	7 -	2 5	ŗ

THE REPORT OF THE PROPERTY OF

0 W	ETA 0.	9.5000	AXIS		UPSILON	0,71756		•	٠	•	0.17989	•	•		•	-0.29802		•	•	-0.66109		٠	•	٠	-	•	-1.27125	-1.34283	-1.40647	-1.41317	-1.41994	1.78181	-1.41186	
2	ÃU o.	RHO	SECTION	LOWER	ALPHA	-0.42131	-0.36214	-0.30338	-0.24497		-0.12900		٠	٠.		0.15829		0.27253		0.38639	•			٠		٠.		0.83030	•	0.67370	0.86957	S UPSILON		
ROTOR	о	AA NOI	WITH ORIGIN AT		UPSILON	0.67375	•	•	.3411	0.23543	0.13288	0.03353	٠		. 2501	-0.34132	-0.43134			-0.69638	-0.78310	-0.86886	-0.95375	-1.03798	-1.12162	-1.20468	-1.28742	-1.35639	-1.41770	-1.42147	-1.41994	ALPHA -1.08535	. 0	
STAGE 1.	2 -7.03620	SECTION	COORDINATES &	UPPER	ALPHA	-0.50554	-0.44709		-0.32902	-0.26952	-0.20976	-0.14982	-0.08976		•	0.09103	0.15149	0.21203	0.27267	0.33340		•	0.51601	•	•	0.69896	0.75997	•	0.85602		0.86957		¥	
	SYSTEM ORIGIN	SECTION NO 1	SURFACE		1/0	0.02524	. 02553	.02561	0.02551	.02525	.02486	.02434	. 02372			0.02127	0.02029	0.01923	0.01811	0.01693	0.01569	0.01441	0.01309			٠	0.00751	0.00631	0.00510	0.00510	0.00510	0.00963	0.00984	
	COORD SY	S			T d	10	9	17	•	9	50	2	25	23	24	22	56	27		8 80		31	32	33	34	35	36	37	38	38	40		TE RAD	

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NB 20	ETA 0.	RHG 8.5000	CAMBER 1.078	7.55250	UPSILON 0.25908 0.25407 0.25407
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	Ð.			SURFACE ARC LENGTH	ALPHA -0.19974 -0.19877 -0.19877 -0.00100
ROTOR		{		E AF	• • • • •
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	Œ	ō	STAGGER 58.586	2	
÷	120	SECTION AA	S	S	SECTION C.G.
	036	Ŋ			a'N A'L
STAGE	-7.				SECTION C.G. STREAMSURFACE SECTION BLADE AXIS STACKING AXIS (RADIAL)
ST	N				SE(
	7	-		03	CE (1S
	10	9		0.263103	SECTION C.G. Streamsurface Blade axis Stacking axis
	8	SECTION NO	0 :0	Ö	SECTION C.(STREAMSURF/ BLADE AXIS STACKING A)
	Ë	Ĭ	CHORD 3.7610		REA ADE ACK
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	COORD SYSTEM ORIGIN Z -7.03620				

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	ETA	8.0000																						•	ZETA*	088	779	522	187	816	432	028	.601	.067	. 455	642	. 624	. 365	41	. 153	. 355	-
20				UPSILON	75041	7803	52596	36397	9166	99106	76325	53447	1367	0566	9906	28036	46660	65011	3087	0820	18045	34551	47626	AXI	Z	54	2	52	56.	36	57	8	28	29	9	29.	28	20	28	28.	~	26.
2	ö	S. D.		UPS	1.7	1.6		•		6.0	0.7				•	•	4.0-	•	•	•	-1.1	-1.3	-1.4	SECTION AXIS	Z.	=	2	53	36	=	4	4	4	9	22	<u> </u>	9 !	7	8:	စ္က	8	စ္က
	£			^																				AT SE	UPSILON	. 75041	.67320	. 59385	. 512;	.42891	•	-	•		. 96352				. 51400			. 1988
			DATA	THICKNESS	01903	2912	04746	06331	07662	08817	9682	10141	0236	0031	09595	08967	08182	07267	6252	05170	ĸ	2939	02031		J	_	-	_	-	-	,	# * (,	- (0 (.	0	0	0 (0	0	D
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	œ	SECTION		*	€0	4	0	9	a	0	4	ın.	e e	е	9	0	ဗ	4	80	G)	6 0	o	0	¥13	ALPHA	1.193	1.14025	•	1.02977			0.86405				•	55471	•		.35	. 28	0.223
-	-7.03620	SEC	MEANL I NE	ZETA		•	•			59.380	9.674		•	•	54.466	•	•	e.		٦.	8	. 73	50.78	ATES		•	-	7	ī	o ·	P	o O	7	P	o (?	o (ĭ	o (P	7	7
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v)	N -	~		<u>∢</u>	49	99	88	4	22	ည္	80	47	99	68	33	53	88	2	07	-	N	80	=		1/0			<u>.</u>	•	0.01	•			•			•	•	9	9	0.	0.025
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	EM Q	SECTION			•	7	ī	o P	7	o.	o ·	o.	P	o P	~	_	_	•	•	•	Ü		•	ME/	PCT AL		.0220	.0500	. 0750	1000	1250	1500	2007	2000	0000	Z POC	2900	3200	3500	Ф.		4400
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	COURD																				6;	2			P.		8	ო	4	1 0 (9 1	~ •	D (3 1 (2;		2 .	<u> </u>	<u>.</u> .	0 (9 !) [

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50	ETA	8.0000	AXIS	ZETA*	•	•	•	54.179	53.953	33. GC	90.00	20.00 20.00		53.410	53,366				٠			50.780	8ER 308	AXIS		5		_			<u>.</u>	_	_		<u>-</u> -	<u>-</u> (.	öö
2	ö	E	SECTION	N N	122	147	9 1	e e	96	9 1	- 0	8 -	74	0	98	31	164	14	28	59	03	929	CAMBER 3.308	SECTION AXIS	LOWER	ALPHA	19549	18758	18176	12809	.06863	95050	. 89186	83349	77539	71762	040	51263
	£		¥	UPSILON	0.10022	ö	0	ö		10.35378	; c	ċc				0		•	•	-1.33859	-1.4080	~		AT		<	-	7	÷			: q	ģ	Ģ.		•	•	į
ROTOR	o.	88	LITH ORIGIN	⋖	98	69	40	e !	<u> </u>	4 K	2 2	2 2	16	06	a	48	92	25	34	53	87		<i>~</i> ~	COGRDINATES WITH ORIGIN		UPSILON	75041	74364	73681	66462	58260 40876	11321	32592	23687	. 14604	5352	0 C C C C C C C C C C C C C C C C C C C	71282
÷.	e 0	SECTION		ALPHA	•		•	9	0.10817	0.17440							_		-	0.9036	_	014	STAGGER 55.597	S WITH	UPPER		-	•	•	•	-	-	`	-	•	- 0	•	
9 E	-7.03620	S	COORDINATES		е	ю·	4	.	D 4	D P		· C		10	0	a	ю	•	٠.	**	_	o	••) I NATE	S	ALPHA	9549	9926	9086	5241		99854	94671	19461	1222	78952	7.6350 66156	9678
STAGE	N	8		1/0		0.02515		0.02383		0.02200					0.01490			•	8	.007	0.00641	0.00519				AL	-	Ξ.	- '	٦,		6-0-	9	•	•	-0-7	; c	
	GRIGIN	D Z	MEANL I WE	AL					0000													0000	04	SURFACE		ပ	00487	00487	00487	19/00	01016	467	01664	842	200	02143	02404	1 4 6 6 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4
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50	ETA 0.	8.0000	1.5		UPSILGN	0.65036		•	•	0.22688	•		-0.06131		-0.24650		٠		-0.61231	-0.70330	-0.79418	-0.88200	-0.97552	•	-1.15459	•	-1.32935	-1.40018	-1.46183	-1.46887	-1.47626	1 74294	-1.46616
NB	MU 0.	R. F. C.	T SECTION AXIS	LOWER	ALPHA	-0.44537	-0.37864		-0.24648		-0.11559					0.20830	0.27395		0.40289		0.53142	0.59556	0.65961	0.72359	٠		•	-	1.01579	1.01792	1.01411		1 UPSILON
. ROTOR	o œ	SECTION BB	WITH ORIGIN AT	ER	UPSILON	0.59938		0.37879								٠	-0.47856			-0.74418		-0.91976	-1.00711	-1.09383	-1.17969	-1.26449	-1.34783	-1.41588	-1.47499	-1.47849	-1.47626	ADDIT - 1 180K	
STAGE	2 -7.03620	2 SEC	E COORDINATES	UPPER	ALPHA	-0.53146	.4656	-0.39932		-0.26562	-0.19836	-0.13096	-0.06347	٠	0.07181	•	0.20755	•	0.34376	0.41203	0.48038	0.54881	0.61734	0.68594	0 75457	0.82323	0.89190	0.84809	0.99960	1.00593	1.01411	+	CENTER AT A
	SYSTEM ORIGIN	SECTION NO	SURFACE		1/0	0.02559	,	•		0.02597		0.02515		0.02383			•		0.01880	•		0.01490	•	0.01205	•	0.00912	0.00764			0.00519			RAD 0.01043
	COORD :				F	10	10	17	18	19	50	2	22	23	24	20	26	27	28	6 7		31	32	33	34	35	36	37	38	38	40		1 1 1 1

STAGE 1. RGTGR NB 20 CGGRD SYSTEM GRIGIN Z -7.03620 R 0. MU 0. ETA 0. SECTION NG 2 SECTION BB RHG 8.0000 CHGRD STAGGER CAMBER 3.9107 55.597 3.308 AREA 0.288309 SURFACE ARC LENGTH 7.85357						
MU O. MU O. ARC LENGTH	20	ETA 0.	8.0000	308	85357	
MU MU S	9	o.	SH P	CAM 3.:		
COGRD	STAGE 1. ROTOR	.	N			YI DIY
		COORE				

UPSILGN 0.19135 0.19120 0.19120	
ALPHA -0.18399 -0.18485 -0.18485	
SECTION C.G. STREAMSURFACE SECTION C.G. BLADE AXIS STACKING AXIS (RADIAL)	

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50	ETA	7.5000		LON	047	63559	47934	.31448	14146	34333 72266	50530	30075	.11111	737	010	4102/	57877	200	91216	23717	200	AXIS	ZETA*	52.349	53.030	53.634				55.673 56.023		56.518				.67	53.613	•	•
2	ö	E.		UPSILON	1.71		1.47	1.31	- · · · · · · · · · · · · · · · · · · ·	0.00	0.0	•	•			•	ဂု ငှ	•			•	SECTION AXIS	UPSILON	71047	63038	54841	46466	37921	29210	. 20343 11346	2243	91215	0137	69124	58295	47772	7638	368∠	8541
œ	æ		DATA	THICKNESS	01980	03111	05208	07071	08676	11236	11689	12097	11928	11456	10736	90980	08711	20100	04768	03366	220	ORIGIN AT	UPS	1.7	1.6	1.0	4.				•		•	•	•	0.47	•	ú	
ROTOR	٠. ن	S NO	INPUT	THE						.	ö	Ö	0	0	_	_	_	_ `	٠.		0	WITH OR	ALPHA	29948	23846	7744	1642	5540	2000	87235	11133	3811	6488	59166	1844	44522	17200	9877	N
	-7.03620	SECTION	MEANLINE	ZETA*				55.094	55.898 56.436					oi (48.742		46.373	•	o co	7.6	6.84		¥	-1.2	-1.2	-		-1.0	2 (-0.8	-0.7	-0.6	D. O-		•	•	•	-0.2
STAGE	.7- 5	ო	Æ	•	48	38	င္ပ	96	ر د د د د	9 6	99	39	47	<u>0</u>	\ .	- 9	7 6	- d	00		27	E COORDINATES	1/0		•			0.01624	•	0.02267			•	0.02892	•	0.03040			
	SYSTEM ORIGIN	N N N		ALPHA	-1.2994		, ,	-1.00996	-0.89125 -0.75889	• ~			-0.165		0.13507	•	•	73050	0.8769	021	4	MEANL I NE	AL							1750							00	8	
		SECTION		e	-	~	ლ [,]	4 1	ب در	^	. 60	œ	<u>o</u> ;	- (N C) \	4 K	9 4	- 2	18	0		PCT		•	•	•	•		- - -		•	•	•	•			4	4
	COORD																	e	66				P	-	~	თ [,]	4 (in u	10	. 60	O)	10	=	75	13	4 1	2	16	17

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	ó	000			•	•	•	~	_		A.	"	_	•	_		"	**	~	"	"	e.	•				UPSILON	71047	.71251	. 70905	.63996	. 56123	.48042	. 39763	.31290	. 22638	13834	900	940	4 (2)	72282
20	ETA	7.5000	AXIS	ZETA*	50.493	•	o ·	œ.		6	48.482		ė	•	ė	•	٠	48.354	•	•	47.736		46.848	ă	68	AXIS	בֿ	_	-	<u>-</u>								<u>-</u> (o
2	MU 0.	S. S.	SECTION	UPSILON	•	.00755					.41242							•	.07186	534	344	5	.36700	CAMBER	5.500	AT SECTION A	ALPHA	-1.29948	-1.29131	-1.28512	-1.22573	-1.16003	•		-0.96441			o (0.6951	9.618	-0.54447
ROTOR	0	ON CC	WITH ORIGIN AT	ALPHA U	15233 0	07911		6734	056					50667	•	65312	72634 -	- 93664	87278 -	- 109	- 626	08025 -1	14127 -1	0000	51.582	WITH ORIGIN A	UPSILON	1.71047	1.70329	1.69624	1.62079	1.53558	•	•	1.27129	•	•	•	o r	•	0.65965
STAGE 1.	2 -7.03620	SECTION	COGRDINATES W	T/C A	03029 -0.	•	02907 -0.				02494 0.		ö	ö	ö				01224 0.		980		00562 1.	AT.S.	51	COORDINATES W	ALPHA	-1,29948	_	_	-1.25119		•	•		-0.96693	•	ö,	0.7810	. 710	-0.63886
	SYSTEM ORIGIN	SECTION NO 3	MEANLINE	PCT AL	.4700 0.	ö	. 5300 0.	. 5600 0.	. 5900 0.	.6200 0.	.6500 0.	.6800 0.	.7100 0.	. 7400 0.	.7700 0.	. 8000	.8300 0.	. 8600 0.	.8900 0.	.9200 0.	. 9500 0.	.9750 0.	1.0000 0.		3.9279	SURFACE	1/0	0.00504				0.01101	0.01372	•	•	9		٠.	0.02622	•	0.02892
	COORD S			F.	18	9	20	2	25	23	24	22	26	27	58	58	30	31	35		7		36				P	•	۰ ۵	က	4	SO.	9	7	60	O)	0	-	2 5	. 3	4

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	ETA 0.	7.5000	S		UPSILON	0.61602	0.51224	0.41217	0.31561	0.22292	•	0.04532		•			_			-0.63294	-0.71744	•		•	-1.05584		-1.22304	-1.29176	-1.35117	-1.35866	-1.36700	. 20213	-1 35867	
NB 20	∄ ∪ 0.	SH SH	T SECTION AXIS	LOWER	A.PHA	-0.47014	-0.39651	-0.32342	•			-0.03449	-	0.10915					0.46605			•	٠	0.82013	•	•	•	1.09055	1.14207	1.14488	1.14127	7011		
. ROTOR	o æ	SECTION CC	WITH ORIGIN AT	ER	UPSILON	0.54989	0.44320	0.34059	•		0.05728	-0.03022	•		•	-0.36354	-0.44488	-0.52581	-0.60645	-0.68692	-0.76730	•	٠	٠	-1.08788	-1.16721	-1.24584	-1.31071	-1.36673	-1.37005	-1.36700	7	ALTIA LISSON	(
STAGE	Z -7.03620	3 SEC	E COORDINATES	UPPER	ALPHA	-0.56674	.4939	Ä		-0.27261							0.25034	0.32553	0.40085		0.55183	•	٠.	Ċ	•	0.93077	1.00668	1.06994	1.12539	1.13255	_	+	A TA GRINAC	ī
	SYSTEM ORIGIN	SECTION NO	SURFACE		1/0	0.02980	0.03040	0.03072	0.03079	0.03064	0.03029	•		0.02823	•		•	0.02362	•	•	0.01911	•	٠	0.01402	Ö	•	0.00863	•	•	•	0.00562	C	RAD 0.01033	;
	COORD 8				Ρđ	E.	16	17	18	<u>o</u>	50	2	CI CI	23	24	52	56	27	58	50	06 6		35	33	34	33	36	37	38	38	40		L U	

O	ETA 0.	7.5000	K O	553	
NB 20	ó	SHO DH	CAMBER 5.500	7.89553	
1. ROTOR	03620 R 0. MU	SECTION CC	STAGGER 51.582	SURFACE ARC LENGTH	
STAGE	COORD SYSTEM ORIGIN Z -7.03620 R 0.	SECTION NO 3	CHØRD 3.9279	AREA 0.336214	

UPSILON	0.19023	0.20195	0.20195	Ö
ALPHA	-0.18161	-0.19593	-0.19593	-0.00100
	SECTION C.G.	SIREAMSURFACE SECTION C.G.	BLADE AXIS	STACKING AXIS (RADIAL)

	ö	0																																								
20	ETA	7.0000		NO.	64278	342	40848	131	547	325	360	277	141	13667			-	965	96	3931	891	758	683	AXIS	ZETA*	50.828						•	53.103			52.665	•		o i	B	46.667	45.537
2	ö	RHO		UPSILON	1.642	1.5664	1.406	•	•		0.67992		0.30241	٠	•	-0.17044	•		φ.	۲.	0.87	-1.007	-1.116	SECTION A	NO.	278	56098	47784	39337	765	102	378	504	302	247	74778	518	583	5082		467	741
	₽		T.A.	NESS	000	383	066	08355	436	356	953	974	5424	5363	871	14011	835	396	742	929	966	980	255	A	UPSILON	1.642	1.560	1.47	1.39	1.3076	1.221	1.13	•	•	•	0.747	•	•	0.450	36	0.272	5
ROTOR	ó	0 2	INPUT DATA	THICKNESS		•	•	0.08		•	•	•	_					0.1	•	0.07	•	•	0.02	TH ORIGIN	ALPHA	38949	32348	5747	. 19146	12545	5943	9342	92741	5140	8219	70297	2376	54455	46533	- 1	30690	5769
-	.03627 R	SECTION	MEANLINE 1	ZETA*	0.828	•							•	•	•	2.583	•			ი.	. 84	9.414	9.072	ATES WITH	ALI	•	•			•	•		•	o.	ö	o (o.	ö	Ö	0	٠	-0.2
STAGE	z -7.0		MEA	••	ũ	in	52					4	₫ '	4.		42			4	4		ř		COORDINATES	1/0	00524	00911	01280	01629	11959	32268	02555	2818	03058	03313	03531	03710	38	395	601	4 4	04042
	GRIGIN	Š 4		ALPHA	•	•	•	•	. 94952				•	17236	•	•	•	.47340	•	. 7959	.9568	. 11744	. 25096	MEANLINE		ö	ö	ö	Ö	o	o.	Ö	Ö	ö	o.	Ö	o	ö	ი		0 0	0
	SYSTEM OR	SECTION			-									0		0 (_	_	MEA	PCT AL		•	•	•	•			•			0.2600			0.3500			44
	COORD SY	5 7		4	-	W	6	4	IO.	Ð	~	•		5	_ ;			4		_	70	-	2		PT	-	N	ო	4	IO.	9	^	₩ .	O)	0	- (2	က	4 1	ი (9 7	<u>`</u>

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STAGE

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ETA 0.	7.0000	AXIS	ZETA*	•	43.952	•	-	42.495		•	41.555	41.301			•	40.297		39.815	39.597	39.448	Ġ	39.072	2	36	IXIS		UPSILGN	1.64278	1.64510	1.64160	1.57165	1.49296	1.41243		1.16316	1.07835	0.00304	8905	0.78868	0.68886
بر من :	RHO	AT SECTION	UPSILON	0.11297	•	•		•	-0.25932		•	•		٠	-		•			.0088	. 063	-1.11683	RAMAC	11.756	N AT SECTION AXIS	LOVER	ALPHA	-1.38949		٠	•	-1.23827	-1.1558/	4.08374	•				-0.64936	-0.56798
20 R O.	SECTION DD	ES WITH ORIGIN	ALPHA	-0.14848	٠.	٠	٠.						0.56445					0.96051	•	1.11894	. 1849	1.25096	STAGGER	46.264	ES WITH ORIGIN	lippen.	UPSILON	1.84278	1.63537	1.62829			1.3/431	- 20462 · ·			٠ _ ٠		٠	0.60150
N Z -7.03620	4	NE COORDINATES	1/0	0.04010		•	0.03764	•	0.03492	•	•	•	0.02745	•	0.02296	•	•	<u></u>	.013	<u></u>	.008	. 003			CE COORDINATES		ALPHA	-1.38949	•	-1.39152	•	•		- (•	•		-0.83275		-0.67954
SYSTEM ORIGIN		MEANL I NE	PCT AL	•	0.5000	•	•	0.5900		•	•	•	0.7400	•	•	•	•	•	•	-	0.8720	1.0000	CHO	3.8194	SURFACE		1/0	٠.	•			•	0.01629	•	. c			0.03313	9	. 037
COORD			PT	-	9	50	21	22	23	24	10 10 10 10 10 10 10 10 10 10 10 10 10 1	58	27	58	5 8	30	31	35	33		က် 71						PT	-	8	ო	4	in (10 t	` •	0 0	9 0		. 4	13	4

	·o	000			UPSILGN	•	.49988	•		. 24647	.16744	. 09001		.06147	. 13598	. 20987	. 28324	•	.42868	. 50081	. 57249	. 64371	. 71452	. 78491			. 99352	.05097	. 10055	. 10778	.11683	.63444	. 10935
	ETA	7.0000	S		3	0	0	0	0	0	ó	0	0	P	ó	ç	ó	0	o	ė.	ö	o o	o	ó	P	P	ó				ī	_	7
20			AX1S																													z	Z
Z Z	ö	5	SECTION	LOWER	ALPHA	.48752	40801	32914		17261	09465	.01689	06070	13810	21530	29233	. 36919	.44590	. 52246	59888	.67517	. 75136	. 82750	. 90356	. 97957	.05555	. 13152	•	N	. 25351	ത	UPSTLON	UPSILON
	⊋					9	ò	ó	o.	o O	0		o	o	o	o			o	ö		o	o	o	o O		_	-	_		<u>-</u>	_	. w
	_		GIN AT		z	9	9	œ.	7	4	0	ın	0	80	8	9	S)	4	၈	60	C)	9	ın	1 0	7	0	0	4	8	o,	၉	38271	.24176
ROTOR	o.	8	WITH ORIGIN		UPSILON	4994	40176	30929	22167	13834	02820	01865	09360	16678	23842	30876	37795	44614	51343	57988	64552	7103	77445	83785	3005	96260	02410	07504	.11892	12119	11683	7	
8	œ	Z	I TH		Š	ò	·		٠			•							•		•	•			9.0	0	-	-1.0	-	-1.1	-	Ą	Ξ¥
÷		SECTION	X S	UPPER																												AI PHA	ALPHA
	-7.03620	S	COORDINATES	בֿ	⋖	57	99	0	90	78	30	64	80	23	4 10	82	42	4	8	02	5	38	68	40	46	90	36	0	75	256	96		A
STAGE	-7.		SRD1		ALPHA	601	52266	44310	36308	28278	20230	. 12164	04080	04023	12145	20285	28442	36614	44800	530	61215	69438	77668	.65904	941	.02390	. 10636	.17510	. 23475	242	250	SHVED	CENTER
S	N	4				Ó	o	o	o	o	o O	0	0	0	0	o	0	o	0	o	O	o	o	0	o		-	-	_	•	-	Ü	Ü
	Z		SURFACE																													ĸ	ရွ
	OR 10	Z	SURF		ပ	03850	03951	04015	04044	04042	04010	03952	03869	03764	03638	03492	03328	03148	02954	02745	02526	02296	02057	01811	558	01300	01037	00815	00591	00591	591	5	01186
	Ψ	SECTION			1/0	-		-			•					•			•		•		•	0	6	9	•					c	0
	SYSTEM ORIGIN	SEC				0	0	0	٥	0	0	J	J	J	J	0	J	J	0	O	O	J	U	U	J	O	0	0	0	J	0	0	RAD
	COURD				d.	50	16	17	18	9	80	2	22	23	24	25	26	27	28	28	30	3	32	33	34	35	36	37	38	39	40	u -	l H
	ၓ																																

2	ETA 0.	7.0000	CAMBER 11.756	7.70075	ON 171 171
ĝ	o.	S. E.	CAM 11.		UPSILGN 0.21303 0.22671 0.22671 0.
מסי	J.	Ω0		SURFACE ARC LENGTH	ALPHA -0.18156 -0.20669 -0.20669
1. ROTOR	520 R O.	SECTION DD	STAGGER 46.264	SURFACE	0.
STAGE	z -7.03	_		•	SECTION
	1 ORIGIN	SECTION NO 4	CHÖRD 3.8194	0.410323	SECTION C.G. STREAMSURFACE SECTION C.G. BLADE AXIS (RADIAL)
	COORD SYSTEM ORIGIN Z -7.03620 R 0.	SECTI	CHG 3.6	AREA	SEC

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	ö	8														•							
20	ETA	6.5000		Z O	603	20	2	8	99	9	77	61	34	34	32	03	63	-	35	82	34	2	24
2	ö	S. F.		UPSILON	1.55303	1.47607	1.31821	1.15593	0.99066	0.80519	0.61877	0.44261	0.28234	0.13454	-0.00432	-0.13605	-0.26163	-0.38211	-0.49835	-0.61082	-0.71934	-0.82391	-0.90624
	⊋			1 0																			
ROTOR	o.	EE	UT DATA	THI CKNESS	0.01980	0.03708	0.07001	0.10029	0.12738			0.18651	0.19600	0.19688	0.19175	0.18145	0.16670	0.14821		•	0.07563	0.04729	0.02250
Œ	œ	Š	Z .																				
STAGE 1.	-7.03620	SECTION	MEANLINE INPUT DATA	ZETA*	49.438	49.781	50.354	50.726	50.731	49.941	47.928	45.081	42.276	40.154	38,456	36.956	35.862	34.566	33.618	32 667	31.662	30.662	29.810
in .	SYSTEM ORIGIN Z	SECTION NO 5		ALPHA	-1.46638	-1.40097	-1.26902	-1.13561	-1.00078	-0.85084	-0.68548	-0.51867	-0.35051	-0.18141		0.15906	0.33009	0.50156	0.67339	0.84557	1.01820	1.19132	1.33601
		SE		g. 1-	-	α.	က	4	8 7	9	^	•	a	<u>.</u>	- -	2	ი	7	E	16	^	9	9
	COORD																				;	4	

MEANLINE COORDINATES WITH ORIGIN AT SECTION AXIS

)	ZETA*	49.438		50, 154		50.628					49.660			46.008			41.803	
	UPSILON	1.55303	1.47057	1.39708	1.30272	1.21764	1.13202	1.04610	0.96031	0.87519	0.77486	0.67748	0.58386	0.49455	0.40975	0.32929	0.25249	0.17877
	ALPHA	-1.46638	-1.39632	-1.32626	-1.25620	-1.18614	-1.11608	-1.04602	-0.97596	-0.90590	-0.82183	-0.73776	-0.65369	-0.56962	-0.48555	-0.40147	-0.31740	-0.23333
	1/0	0.00531	0.01027	0.01504	0.01959	0.02392	0.02800	0.03183	0.03537	0.03862	0.04209	0.04507	0.04756	0.04956	0.05108	0.05213	0.05273	0.05289
	PCT AL	°.	0.0250	0.0500	0.0220	0.1000	0.1250	0.1500	0.1750	0.2000	0.2300	0.2600	0.2900	0.3200	0.3500	0.3800	0.410C	0.4400
	F	-	Ø	ო	4	N)	9	^	€	O)	0	-	12	13	4	<u>.</u>	16	17

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THE RESIDENCE ASSESSED AND ASSESSED AND ASSESSED ASSESSED ASSESSED ASSESSED ASSESSED ASSESSED ASSESSED ASSESSED.

																											ND	80	67	52	20	4	9	7	2	[9]	p== (13	67	D 1	` B
0	000		*	•	a	ю	_	e	_	4	_	6	e	e		6	a	0	a	0	ю :	0					UPSILON	. 55303	. 555	. 55252	. 482	. 405	. 32599	. 24594	. 16504	.08361	٠	٠	. 82567	73288	. 643
ETA	6.5000	AXIS	ZETA		O)	•	37.417		•		•	34.433		33.523			•	٠	•	٠	30, 225		CAMBER	.628	AXIS		5	-	_	•	_	_	-				,	0	0 (D
ö	S. S.	SECTION	Z,	10761	365	332	350	00	398	926	996	39706	110	34	56558	191	302	521	77639	562	226	324	Ą.	9	SECTION	LOWER	ALPHA	46638	45830	45180	. 38169	.30473	. 22805	. 15166	.07563	.0000	. 92492	85044	8	746	. 58837
2		¥	UPSILON	0.107	•							-0.397							•	•	•	-0.90			¥		•	-	7		7	7	7			7	o	ဂ္	0	0	0
.:	EE	GRIGIN		9	3 1	6	9	<u>ო</u>	0	4	4	2	9	46	5	o	7.	ĵ,	2	ص ص	ιŭ	=	_		ORIGIN		UPSILON	55303	54555	53855	45822	36911	. 27944	10935	00660	00828	91852	82924	240	219	2382
a c	SECTION	VI TH	ALPHA	0.14926	0.06519	0.01889	0.10296			0.35517	0.43924			. 691	. 775	0.85960	•	1.02775	1.11182	1.19589	65	1.3360	TAGGER	41.292	HHIM	FE 70			-	. .	7.	-		•	-	•	•	•	0.7		o.
-7.03620	SEC	COORDINATES		ī	ī	-	_																V.) `	COORDINATES WITH	UPPER		46638	47014	46815	41095	34779	28436	22062	654	09203	02701	96136	88166	80089	901
7- 2	R)	COORD	1/0	.05264	.05200	.05101	.04970	.04808	.04618	.04403	.04164	.03904	.03625	.05327	.03012	.02683	.02341	.01987	.01622	.01247	.00927	. 00603					ALPHA	-1.46	-1.47	-1,46	-1.41	•	-1.28	•	•	٠					-0.71
ž	9	MEANL I NE		0	0	0	0	0	0	0	0	0	0	0	٥	0	0	0	0	٥	0	0			SURFACE								_	•	_	_		•	_		"
M GRI	SECTION N	MEAN	T AL	4700	5000	5300	5600	5900	6200	6500	6800	7100	7400	7700	8000	8300	8600	8900	9200	5500	9750	0000		7298	SUR		1/0	00531	00531	00531	01027	01504	01959	02392	02800	03183	03537	03862	04209	4	04756
SYSTEM ORIGIN	SECT		PCT	o.	Ö	0				o				•		•	•	•	•	ö	o.	<u>-</u>	Ç					o.	Ö	o	Ö	o.	Ö	o	•	•	•	Ö	Ö	Ö	o .
COORD			Ā		9	80	2	22	83	24	25	(3	27	28	8	30	31	32	33		နှင့် 75						P	-	N	က	4	N)	9	7	æ	σ			2		<u>.</u> 4
																						,																			

414		6.5000	AX18		UPSILGN	0.55675	0.47773	0.40034	•	•		0.11409	0.04648	-0.01989	-0.08514		•			•		-0.51849	-0.57765		-0.69365		-0.80660		-0.89219	-0.89886	-0.90824	1.54483	-0.90221
2	.; ⊇	RHO	SECTION	LOWER	ALPHA	-0.50312	-0.41881	-0.33512	-0.25185		-	-0.00423		•	•	•	٠	•	•	•	•	•	٠	0.96686	•	1.12744	1.20774	1.27465	1.33230	1.33714	1.33601	UPSILON	
٥	E	SECTION EE	WITH GRIBIN AT	ER	UPSILON	0.43035	0.34177	0.25823	0.17919	•		-0.03678		•						-0.51024	-0.56206	-0.61264		-0.71001		-0.80231	-0.84663	-0.88270	-0.91314	-0.91400	-0.90824	ALPHA -1.45937	
	7 -7.03620	5 SEC	COORDINATES	UPFER	ALPHA	-0.63612	-0.55228		-0.38295			-0.12614	-0.03989	•	0.13342	0.22038	•	0.39477		0.56963		0.74488	•	0.92049	1.008:14	1.09619	1.18404	1.25725	1.32026	1.32834	1.33601		ΤV
2000	SYSIEM ORIGIN	SECTION NO	SURFACE		1/0	0.04956	0.05108	•	0.05273	0.05289	•	0.05200	0.05101		0.04808	0.04618	٠	0.04164	0.03904	0.03625		0.03012	٠.	0.02341	٠	0.01622	•	0.00927	0.00603	0.00603	0.00603	RAD 0.01080	c
	ממאמ				PT	<u>.</u>	16	17	18	9	50	21	22	23	24	20	56	27	28		၉ 76		32	33	34	33	36	37	38	38	40		u

	ö	0			
20	ETA	6.5000	£ 60	619	**
<u>2</u>	ö.	Z E	CAMBER 19.628	7.55619	UPSILGN 0.20846 0.21662 0.21662 0.2000
	Ð			SURFACE ARC LENGTH	ALPHA -0.18296 -0.21253 -0.21253 -0.0100
ROTOR	ö	EE	92 92	ACE AR	• 0000
<u>.</u>	320 R	SECTION EE	STAGGER 41.292	SURF	0.
SIAGE 1. ROTOR	-7.036	•/			ECTION RADIAL)
•	COORD SYSTEM ORIGIN Z -7.03620 R 0.	SECTION NO 5	RD 298	0.505076	SECTION C.G. Streamsurface Section C.G. Blade axis Stacking axis (Radial)
	SYSTEM	SECTI	CHGRD 3.7298	APEA	SECT STRE/ BLADE
	COORD				

PHASE I ROTOR

	o.	8																					
6	ETA	6.0000		7	_						•	_	_				_			_			_
20		Ð		UPSILON	44821	37084	2130	1.05242	0.89181	0.72057	0.54779	0.39209	0.25074	0.11974	-0.00326	-0.11666	-0.22668	-0.32781	-0.42265	-0.51139	-0.59405	-0.67038	-0.72874
Š	ö	S. F.		a.	-	_	_	_	0	0	0	ö	0	o	0	0	0	0	0	-0	0	Ö	9
	£			S																			
ROTOR		Ħ	T DATA	THI CKNESS	0.01899	0.03919	0.07765	5.11314	0.14509	0.17520	3.20112	0.21955	0.23043	3.23352	0.22903	3.21787	0.20091	0.17894	0.15269	0.12274	0.08964	0.05384	0.02220
5	o.		INPU	F		Ŭ	Ū									Ü	Ü	Ü	J	Ü	O	O	0
Ē 1.	-7.03620	SECTION	MEANLINE INPUT DATA	ZETA*	48.313	48.571	48.936	46.944	48.298	46.454	43.360	40.185	37.577	35.597	33.809	31.986	30.211	28,523	26.890	25, 238	23,507	21.625	19.852
STAGE	7- 2		Σ																				
		9		ALPHA	. 53207	.46347	.32501	.18517	-1.04390	88705	-0.71414	-0.53984	-0.36436	16784	-0.01043	16786	34685	0.52659	70719	88855	96020	25457	40862
	SYSTEM ORIGIN	SECTION			-	7	7	7	7	٠ <u></u>	o	o	o	o O	o	Ö	0	o O	0	ö	_	_	-
	SYSTI	SEC.		F	-	CV	က	4	ю	ဖ	^	•	O	5	=	2	ი	4	<u>.</u>	16	17	9	9
	COORD																			•	78	,	

MEANLINE COORDINATES WITH ORIGIN AT SECTION AXIS

ZETA*	48.313		48.755		48.983	48.875	48.583	48.088	47.304	45,943	44.383	42.715	41.099	39.598	38.272	37.141	~
UPSILON	1.44821	1.36527	1.28170	1.19759	1.11311	28	0.94490	0.86223	0.78136	0.68788	0.59911	0.51522	0.43606	0.36114	0.28990	0.22173	0.15614
ALPHA	-1.53207	-1.45855	-1.38503	-1.31152	-1.23800	-1.16448	-1.09097	-1.01745	-0.94393	-0.85571	-0.76749		-0.59105				-0.23817
1/0	0.00519	0.01110	0.01678	0.02220	0.02737	0.03227	0.03688	0.04116	0.04509	0.04933	0.05301	0.05614	0.05874	0.06081	0.06235	0.06334	0.06380
PCT AL	o.	0.0250	0.0500	0.0750	0.1000	0.1250	0.1500	0.1750	0.2000	0.2300	0.2600	0.2800	0.3200	0.3500	0.3800	0.4100	0.4400
P	-	લ	ღ	4	IO.	9	7	€0	09	0	-	-	13	4	135	16	17

HOLLEN THE PROPERTY OF THE PRO

	ETA 0.	6.0000	•	ZETA*	. 245	•		. 540	.651	272	. 067	. 256	.457	. 665	. 864	. 030	.217	. 352	.471	٠	•	•			ø		UPSILGN	1.44821	1.45083	1.44608	٠	1.30194	•	1.14080	•	0. 90 90 0	0.83730	•		9) }
20		ъ	N AXIS	N	35	8	33	35		9 6	, 50 V	28	27	56	23	8 2	2	53	25	5	8	9	CAMBER	28.461	N AXIS	~		~	4	6	e	.	0 (u -	- a	٥ م	1 C		. u	σ	•
2	₩ O	RHO	N AT SECTION	UPSILON	0.09278	•	-0.02782	•	-0.14043		-0.2433				-0.47884		•	-0.60020	•	0.673	. 7015	. 728	ď	a	N AT SECTION	SUC	ALPHA	•		-	•	-1.36196	•	•	•	•			-0.69966	Ċ)))
1. ROTOR	20 R O.	SECTION FF	ES WITH ORIGIN	ALPHA	-0.14995	.0617	•	•		0.29116	0.46760						•	٠.	٠	. 2615		1.40862	STAGGER	36.512	ES WITH ORIGIN	UPPER	UPSILON	1.44821	1.44090	1.43421	•	•	•	•	•	0.80027	•	•	0.52981	•	•
STAGE	1 Z -7.03620	S	HE COORDINATES	1/0	0.06373	•	•	•		•	0.03392			•	•	•	•	0.02377	•	•	•	-			E COORDINATES	5	ALPHA	-1.53207	IO.	<u>.</u>		•	·.	0/0/2.1-	· - •		•	•	• •	Ċ	•
	SYSTEM ORIGIN	SECTION NO	MEANLINE	PCT AL		•	•	•	•	0.6200	0.6900			0.7700	•	•	•	0.8900	•	•	•	1.0000	CHORD	3.6588	SURFACE		1/0			0.00519	•	•	•	0.02737	•	0.03668		•		•	•
	COORD			F	18	<u>.</u>	20	2	22	n c	, v	5 6	27	58	28	30	31	35		7 9	က	36					PT	-	N	ო	4	ko (۱ ۵	~ a	o a	, C		- 0	1 5	7	

THE TRANSPORT DESIGNATION OF THE PROPERTY OF T

0	ETA 0.	6.0000	<u>s</u>		UPSILON	0.51705	0.44686	0.37945		0.25040			•		-0.04893							•				-0.60517		-0.58407	-0.71269	-0.71852	-0.72874		1.44037	-0.72447
NB 20	₫ 0.	RHO	F SECTION AXIS	LOWER	ALPHA	-0.52041		-0.34396		•		•					0.42856		0.59723	0.68146		0.84979	•	٠	٠	1.18674	1.27121	1.34172	1.40063	1.40785	1.40862		_ `	7 UPSILON
ROTOR	ö	N FF	WITH ORIGIN AT		UPSILON	0.35508	٠	0.20036	0.12936			-0.06392	٠.			-0.28270		-0.37696		-0,46225					-0.64011	-0.66983	-	0.71906	-0.73640	0.73575	0.72874	•	•	_
STAGE 1.	-7.03620 R	SECTION	COORDINATES WI	UPPER	ALPHA	0.66169		٠.			.21722	. 12692	. 03612	. 05505	. 14653	. 23827		. 42226	. 51441	. 60662	. 69888		.88346					. 32849 -		1.40202	1.40862		⊢	CENTER AT ALPHA
••	SYSTEM ORIGIN Z	SECTION NO 6	SURFACE CO		1/0	0.05874 -(0.06081 -0	0.06235 -0	.06334	.06380	. 06373	.06315	0.06211 -0	. 06063	.05876	. 05651		.05101	.04782	.04436	.04066		. 03259	.02826	-	•	•	•		0.00607	0.00607		0.01049	0.01231
	COORD SYS	SĽ			P	5	16	17	- 18	3	50	21	22	23	24	25	5 6	27		80 80		31	35	33	34	32	36	37	38	39	40		LE RAD	

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9	o.	E E	CAMBER 28.461	7.4	UPSILGN 0.18590 0.18518 0.18518 0.18518
	ĩ			SURFACE ARC LENGTH	
ROTOR		1±.		E ARC	ALPHA -0.17715 -0.20689 -0.00100
	6 C	SECTION FF	STAGGER 36.512	URFACI	
<u>-</u>	03620	SECT	RS	v	N C. G
STAGE	-7.				SECTION (RADIA
	COORD SYSTEM ORIGIN Z -7,03620 R 0.	9		82035	SECTION C.O. STREAMSURFACE SECTION C.O. BLADE AXIS STACKING AXIS (RADIAL)
	EM ORI	SECTION NO	CHGRD 3.6588	AREA 0.582035	SECTION C.O. STREAMSURFAC BLADE AXIS STACKING AXI
	SYST	SEC	ပက	AREA	SE STI
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50	ETA	5.5000		NO.	32779	24933	061	250	881	049	421	391	19587	785	087	029	190	271	570	905	168	140	282
2	ö	S. S.		UPSILON	1.32	1.24	1.09061	0.93250	0.77881	0.62049	0.4642	0.32391	0.19	0.07785	-0.03087	-0.13029	-0.22061	-0.30271	-0.37570	-0.43905	-0.49168	-0.53140	-0.55282
ROTOR	MU MU	90	INPUT DATA	THI CKNESS	0.01613	0.03981	0.08145	0.12037	0.15583	0.18981	0.21998	0.24245	0.25684	0.26263	0.25961	0.24672	0.23101	0.20731	0.17835	0.14457	0.10603	0.06225	0.02107
STAGE 1. RC	-7.03620 R 0	SECTION	MEANLINE INPL	ZETA* 1	47.252	47.348	47.292	46.603	45.028	42.352	38.999	36.087	33.704	508	269	986	734	428	19.916	17.103	13.798	9.780	5.755
5	COORD SYSTEM ORIGIN Z	SECTION NO 7		ALPHA	-1,58098	-1 50868	-1.36318	-1.21584	-1.06693	-0.90161	-0.71977	-0.53666	-0.35271	-0.16800	0.01745	0.20348	0.39017	0.57749	0.76547	C. 95418	1.14336	1.33295	1.49099
	OORD SYST	SEC		P-		CV	က	4	10	ø	7	•	a	10	=	- 2	13	7	<u></u>	919	_	18	<u>.</u>
	O																			O	4		

MEANLINE COORDINATES WITH ORIGIN AT SECTION AXIS

ZETA*	47.252	•	47.411	٠	47.013	•	•	•	43.494	•	•	•	•	35.627	•	33.300	•
UPSILON	1.32779	1.24422	1.16055	1.07715	•	0.91260	•	•	0.68094	•	0.51585	0.44043	0.36924	0.30162	0.23704	0.17521	0.11593
ALPHA	-1.58098	-1.50418	-1.42738	-1.35059	-1.27379	-1.19699	-1.12019	-1.04339		-0.87443	-0.78227		-0.59795		-0.41363	-0.32147	-0.22931
1/0	0.00503	•		0.02357	•		•	0.04471		0.05408	٠	0.06223		0.06814	0.07024	0.07175	0.07266
PCT AL	o.	0.0250	0.0500	0.0750	0.1000	0.1250	0.1500	0.1750	0.2000	0.2300	0.2600	0.2900	0.3200	0.3500	0 3800	0.4100	0.4400
P	-	8	က	4	Ю	ഗ	~	60	Ø	10		12	13	7	<u>.</u>	16	17

20	ETA 0.	5.5000	AXIS	ZETA*	31.118			•	26.647		•		22.164	٠	, M.C		100 C				1.000		•	CAMBER	. 496	AXIS		UPSILON	1.32779	1.33043	•	4.000.4	•			0.88292			•	0.59631	. 528
2	AU O.	RHO	N AT SECTION	UPSILON	0.05909	•				-0.18958	-0.23254	-0.27335	-0.31199	-0.34841						-0.51482	•	. 543	-0.55282	CA	4	AT SECTION	LOWER	ALPHA	•	٠	٠	-1.46800		• •	•	•	-0.98677	•	-0.80945	-0.71443	
1. ROTOR	20 R O.	SECTION 00	ES WITH ORIGIN	ALPHA	-0.13715	-0.04500	•	0.13932	•	0.32364	0.41580			0.69228		•	0.0000	•	•	CA (373	.4141	1.49099	STAGGER	31.474	ES WITH ORIGIN	UPPER	UPSILON	•	1.32072	1.31438	•	10851.	•		0.78261		•	0.52337	•	•
STAGE	N Z -7.03620	8	NE COORDINATES	1/0	•			٠.	C. 06843		-		•	0.05281	•	•	•		•	•		•	•			CE COORDINATES	1	ALPHA		•	<u>,</u>	, ,	<u> </u>	•			<u> </u>	.027	-0.93940	. 850	J
	SYSTEM ORIGIN	SECTION NO	MEANLINE	PCT AL	0.4700	ເຄ	•		0.5900	•		•	٠		٠	•	•	•	•	•	9	975	1.0000	CHORD	3.6019	SURFACE		1/0	0.00503	0.00503	•	•	•	0.0830	•	0.03988			•	0.05844	
	COORD			F	•	0	50	21	22	23	24	20	5 6	27	28	30 Y	30		35	33	83		36					PT		N	၈	4 1	n (9 6	- Œ	O O		-	12	13	4

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	ö	000			UPSILON	.46348	.40137	34139	. 28321	. 22664	. 17155	11790	. 06572	.01499	.03430	٦.		. 17383	.21749	. 25960	30002	. 33877	.37569	41070	.44356	.47404	. 50201	. 52326	53990	. 54430	. 55282	32039	. 55159	
	ETA	5.5000	•		5	Ö	Ö	o	o	o	o	ö	o	o	o	o	o	o	ò	0	ö	o	0	Ö	o	ọ	o	o	o	o	o	_	o	
20	•	•	AXIS																													z	z	
9	÷	S D	SECTION	LOWER	¥	52709	43430	34212	25053	15958	06926	02043	10958	19832	20675	37496	46299	55086	63862	72628	31391	90158	26937	07726	. 16533	25369	34247	.<1696	.48186	48860	6606	UPSTION	UPSILON	
	0		ECI	3	ALPHA	0.5		٠						°. ±	٠	•	•	٠	0.63	•	٠	•	<u>8</u> .0	0	- 16	Ň	.3	<u>.</u>	4.	4	4	5	5	
	Ē		¥			٢	P	P	Ÿ	P	P	U	•	J	J	Ü	J	J	J	J	U	Ü	0		_	_	_	_	_	_	-	57418	.47903	
~			ORIGIN		Z	8	9	6	-	Ξ.	7	6	õ	4	õ	7	7	7	õ	က္က	8	4	ខ្ល	õ	ñ	50	<u>0</u>	_	<u></u>	0	82	ic.	4	
ROTOR	o.	8			UPSILON	27500	20186	13269	0672	00521	05337	10859	16050	20914	254	29697	33637	372	40650	4372	46500	4897	51133	52969	544	55559	56230	56431	56361	56110	225	ī	- •	
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-	Ş	SECTION		UPPER																												AI PHA	ALPHA	
	-7.03620	Š	COORDINATES	5	⋖	18	8	5	42	5	4	8	23	33	2	33	61	90	29	58	97	61	ŭ	22	82	78	32	4 9	33	39	66		Α	
STAGE	-7.		RDI		ALPHA	66881	57728	48515	39242	29905	20504	11042	01525	08033	17621	27233	36861	46506	56162	658	75497	85161	94815	04457	40	236	33232	4114	47935	486	490	711	TER	
18	N	7	8		<	o O	o	0	۰ و	0	ė.	o O	•	•	ö	ö	•	•	•	•	•	٠	ö	-	-	-	-	-	_	-	-	2	CENTER	
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	1810	2	SURFACE			74	4	124	07175	993	94	62	73	32	43	600	333	18	999	18	63	5	36	92	882	22	269	30	882	885	585	000	01203	
	Σ	Ď	0)		1/0	06547	06814	07024	071	07266	07294	07262	07173	07032	06843	60990	06333	06018	03666	55281	04863	04415	03936	03426	02885	023	01697	01150	00585	Ö	00585		0	
	SYSTEM ORIGIN	SECTION				Ö	o	Ö	0	Ö	Ö	ö	Ö	ö	Ö	Ö	ö	Ö	ö	Ö	Ö	ö	Ö	ö	ö	ö	o.	Ö	Ö	Ö	o.	049	RAD	
	COORD				PT	50	9	17	9	6	20	2	22	23	4	23	5 8	2	58	58	30	ဗ	32	33	34	9	36	37	38	39	4	<u>u</u>	П П	
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20	ETA 0.	5.5000	CAMBER 41.496	7.40980	.CN 13.7 18.3
2	ö		CA 41.	7.	UPSILON 0.13937 0.12983 0.12983 0.
ROTOR	D. MU	90	~	SURFACE ARC LENGTH	ALPHA -0.14018 -0.16879 -0.16879 -0.00100
STAGE 1. RC	7.03620 R C	SECTION	S FAGGER 31.474	SURFAC	SECTION C.O. (RADIAL)
	COORD SYSTEM ORIGIN Z -7.03620 R 0.	SECTION NO 7	CHGRD 3.6019	AREA 0.646538	SECTION C.G. STREAMSURFACE SECTION C.G. BLADE AXIS STACKING AXIS (RADIAL)

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20	ETA 0.	5.0000		2
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STAGE 1. ROTOR	-7.03620 R O.	SECTION HH	MEANLINE INPUT DATA	89UNA910H ***
ST	COORD SYSTEM ORIGIN Z -7.03620 R O.	SECTION NO 8		**************************************
	COOR			

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UPSILON	1.18804	1.10902	9	•	0.65112	•	0.36340	•	•	•	-0.07782	•	-0.22915	-0.28735	-0.33252	-0.36280	•	-0.36579	-0.33746
THI CKNESS	. 0189	0.04109	0	0.12521	0.16276	0.19909		Ġ	•	0.28310	•	•	0.25784	•	0.20617	17	7	0.07632	0.02844
ZETA*	•	45.722	.30	44.020		38.679					24.939		19, 105	۲.		σ.	0, 731	٣.	-15.638
ALPHA	-1.58955	œ	\sim	-1.20163	-1.04535	-0.87315	•	-0.49742		-0.12232		0.25202	0.43853	6243	0.80912	. 991	1.17166	1.34671	1.48795
a	•-	ď	က	4	ED.	Ø	~	•	9	0	Ξ	7	13	7	5	16	17	18	3

MEANLINE COORDINATES WITH ORIGIN AT SECTION AXIS

ZETA*	•	45.690	•	•	•	•	•	41.788	•	•	37.266			•		•	•
UPSILON	1.18804	1.10912	1.03042	0.95226	0.87511	0.79963	0.72643	0.65616	O. 58903	0.51761	0.44040	0.37196	0.30685	w	•	0.12953	0.07620
ALPHA	-1.58955	-1.51261	-1.43568	-1.35874	-1.28180	-1.20486	-1.12793	-1.05099	-0.97405	-0.88173	-0.78940	-0.69708	-0.60475	-0.51243	-0.42010	3277	-0.23545
1/0	0.00551	0.01195	.018	0.02444	0.03043		0.04175	•	•	•	0.06249	•	.070	•	0.07728	•	0.08123
PCT AL	o o	0.0220						0.1750						•	0.3800	4	0.4400
F	-	N	က	4	ĸ	9	^	60	Œ	01	=	12	13	4	5	16	17

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50	ETA	5.0000	AXIS	ZETA*	27.984	2.2		•	21.015	19.503	16.205	4	'n		•	4.788	1.563	n (350.0-	-15.638	•	CAMBER 61.426	AXIS		à		•	.		- c	ö	o	ö	o	•	•	j c	;
2	ö	RHO	SECTION	UPSILON	02573	06682	2080	4855	18538	21946	27910	30436	32633	34479	35935	36947	37464	37425	36/33	33746)	61.	SECTION	LOWER	ALPHA	-1.58955	-1.58203	1.57553	1.49792	1.41326	-1.24497	-1.16162	-1.07900	-0.99719	-0.91619	.	10.7244Z	
	£		GIN AT	UPS	0.0			0		o q		-0.9		-0-	•			0			•		ORIGIN AT		z												n c	.
. ROTOR	0	SECTION HH	WITH ORIGIN	ALPHA	-0.14313					0.41082		0.68780	•	0.87245			1.14942	1.24175	1.33407	1.48795	;	STAGE ER 26.367	WI TH	ËR	UPSILON	1.18804	•	٠	•	1.00845			0.67406		י מו	à.	C. G048)
STAGE 1	-7.03620	SEC	COORDINATES	2/	08228		3160	08021	7830	07589	5963	3579	5148	56 66	5123	04533	03874	03146	2339	1801		<i>0</i> ;	COORDINATES	UPPER	ALPHA	1.58955	1.59271	•	1.52730	•	•	•	-	•	1.03192	•	•	
v)	31N Z	6		+	0.0		0	•	0.0	•		0.0	•	•	•	0.0	٠.		0.00				SURFACE CE			7	7	7			•	•	•	•	7	o c	ָר ר	,
	SYSTEM ORIGIN	SECTION NO	MEANLINE	PCT AL	0.4700			-	0.6200	0.6500	7100			•			•	•	00 4	1.5000)))	CHGRD 3.4348	SURF		1/0	0.00551					0.03043			•		.0574	0.06249	0 / 00 .
	COGRD			F G	∞ (2 0	2 12	22	23	4 6	9 6	27	28	58	30	3	32	93	9 6	n 9	3				PT	-	~	က	4	n (۸ ۵	6 0	တ	0	- ;	2 :	2 5	<u>.</u>

set of vectors which would produce the same circulation as the actual blade taking into account the change in streamline radius and meridional velocity. The difference between the deviation angle implied by the data match calculations and the reference deviation angle was then added to the reference deviation angle calculated from the modified Carter's Rule for the Phase I blade. Phase I Rotor deviation angles are shown on Figure 23. A plot of departure angles for each streamsurface section is shown in Figure 24. Once the intrablade work distribution was chosen these departure angles were required to satisfy the desired incidence angles, deviation angles, and passage area ratios. The resulting streamsurface tip section of the Phase I rotor is compared to that of the baseline rotor in Figure 25. The "deviation angle minus reference deviation angle" for the Phase I rotor was kept essentially the same as the data match analysis although there are some small differences. Figure 26 shows the "delta deviation" compared to the data match of the baseline design.

If the performance of a new rotor design is to be accurately evaluated by comparing overall stage performance with the baseline design then it is important that the stator have nearly the same entering conditions in both cases. Figure 27 shows a comparison of the Phase I stator incidence angles with the data match base. As can be seen the differences are small.

Figure 28 shows the radial distribution of Phase I rotor throat margin and compares it to the data match case. The throat margin for a streamsurface blade section is defined here as the percent of excess throat area over and above the minimum theoretical area required to pass the streamtube flow at a throat Mach number of 1.0 and assuming a total pressure loss equivalent to a normal shock at the upstream Mach number. In a rotor the effect of radius change (between the leading edge and throat) on the relative total enthalpy and pressure is included. As can be seen in Figure 27 the Phase I rotor throat margin is nearly identical to that of the data match of the baseline design.

Details of the Phase I rotor design are given in Section VIII.

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	ETA 0.	5.0000			UPSILGN	0.40726	0.35169	·+	•	0.19782	0.15051	0.10501	0.06122	0.01912	-0.02125	-0.05985	-0.09661	-0.13147	-0.16427	-0.19489	-0.22319	-0.24902	-0.27205	. 2918	•	•		-0.32854	-0.32511	-0.32800	-0.33746	1.18054	-0.34185
23	ш	SO.	AXIS																													7	
, <u>6</u>	o.	R D H	SECTION A	LOWER	ALPHA	53565	44236			16710	07682	01281	10191	19057	27881	36672	45433	54171	62884	71583	80276	88967	.97652	. 06360	.15124	. 23974	.32946	.40582	.47024	48125	48795	UPSTLON	UPSILON
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ROTOR	ö	Ī	GRIGIN		UPSILGN	20644	13796	07316	01201	04541	09905	14886	19486	23717	27585	31090	34231	37003	39393	41382	42946	44056	44665	v	44114	42827	40723	38256	35719	35093	33746	-1.5822	1.47172
Ĕ.	œ	SECTION	S WITH	UPPER	S.	0	0	ö			Ö.	ö.	ė.		•		ò			ò	ò.	ò					ò.	_	•	 0	 0	AH DHA	ALPHA
STAGE	z -7.03620	SE	COORDINATES WITH	Đ	ALPHA	.0.67386	-0.58250	4		-0.30381			-0.01886	•	•	0.27028	•	•	10	٠	0.75749	•	0.95302	1.05060	1.14761	1.24376	1.33869	1.41620	1.47861	1.48587	1.48795		¥
		€				•	•	•	•	•	•	•	•																				
	TEM ORIGIN	SECTION NO	SURFACE		1/0	0.07097	0.07441			٠	•		0.08243	0.08160	•	•	•	•		•	•	•	•	Ÿ.	•	٠.		0.01601	0.00828	-	0.00828	C	60
	SYSTEM	SE				_	_	_	_	_	_	_	_	_	_	_	_	_	_	_	_	_	_	•	_	_	_	_	_	_	_	4	RAD
	COCRD				P	5	16	17	18	9	50	2	22	23	24	25	56	27	28	53	30	3	32	33	34	35	36	37	38	39	40	Ī	Н

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50	ETA	5,0000	XER 126	7.19492	₹:	- 5	2	
2	ö	ž Ž	CAMBER 61.426	7.1	UPSILON	0.06193	0.06193	0
	Ð			SURFACE ARC LENGTH	HA.	275	275	100
TOR		Ŧ		E ARC	ALPHA	-0.10275	-0.10	-0.00100
1. ROTOR	0	SECTION HH	STAGGER 26.367	URFACI				
	03620	SECT	S	Ø		O.O.NC		Ç
STAGE	-7.					SECT 1		(RADI)
	7	•		30	_	CE.		S
	ORIGIA	D Z	0 4 8	0.6837	O O NOTECHO	STREAMSURFACE SECTION C.G.	BLADE AXIS	STACKING AXIS (RADIAL)
	COORD SYSTEM ORIGIN Z -7.03620 R 0.	SECTION NO	CHORD 3.4348	AREA 0.683730		STREA	BLADE	STACK
	COORD			•				

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20		•		UPSILON	1123	7411	106	3334	2665	2:	- K	1557	04132	1582	7798	2728	5283	3282	3434	5285	928	3149	SECTION AXIS	Ñ		4	4	43	4 4	4 4	4 4	39	37	35	34	32	ë	500	N C))
2	_•	문		UPSI	•	96.0	•	•	0.00	•	•	• •	o				•		-0.5			٠ <u>٠</u>	ION				_	_							_		_	_		_
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ш	-7.03620	Ŋ	MEANL I NE	ZE	44	44	43	42	9	9 6	3 6	9 0	8	20.	17.	13	oi Oi	က်	ဂု	-13.	-26.	-39.	INAT																	
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8	æ o	SHO.	AT SECTION	UPSILON			-0.08020	-0.11502	0	-0.17631	-0.20262	Ċ		-0.27490						o.	-0.18393	-0.13149	CA	AT SECTION	LOWER		-1.558/4			-1.39039	-1.31012	-1.23018	-1.15074	-1.07197	-0.99389	٠			-0.64301
דטומא		SECTION JJ	S WITH ORIGIN	ALPHA	. 179	.09172	. 003 70	. 06433	.17235	. 25037		52443	61245	70048	78850	. 87652	. 96454	1.05256			96	1.37531	STAGGER	S WITH ORIGIN	UPPER UPSILGN	;	1.04123	• •			0.79793			0.57044	•	0.43004		•	0.20686
STAGE	2 -7.03620	SE	E COORDINATES	1/0	0.09298	. 09439	. 09520				0.09253	•					0		0.04968	0	0.03229	0.02381	•	E COGROINATES WITH	OPI ALPHA		1.55874		-	-	-1.36726	•	-	-1.16530	٠		ກ (ວ (. 8083	-0.77272
	SYSTEM ORIGIN	SECTION NO	MEANL I NE	PCT AL		•	•	•	•	•	0.6300	•					0.8600	•		9	œ.	1.0000	CHORD 3.1597	SURFACE	1/0		0.00665	0.00665		•				•	9	•		90.	0.07266
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-	Ó		SECTION	5	ALPHA	. 5534	.46	.37		8	-	8	•	٠	•	•	•	•	•	Ÿ.	۲.	٠	.87	8	.03	. 118	. 20%	. 27:	.3208	.3510	.37:	Š	P.
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	2 R	Z	ง		1/0	07737	08157	08526	08840	96060	09298	09439	09520	09541	09503	09407	09253	09043	08776	08449	08061	07608	07084	06479	05779	04968	04051	03228	0238	0238	3238	•	0. 9
	SYSTEM ORIGIN	SECTION			•	0.0	٠	•	•	0.	٠	•	•	٠	٠	•	•	•	0.	•	•	•	•	•	0.	•		•	•	ö	0		RAD
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1. ROTOR	03620	SECT	ST	v
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	COORD SYSTEM ORIGIN Z -7.03620 R 0.	SECTION NO	CHGRD 3.1597	AREA 0.701158
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PS1LON 0.03982 0.00502 0.00502 0.

ALPHA -0.05003 -0.05164 -0.05164

> SECTION C.O. STREAMSURFACE SECTION C.O. BLADE AXIS STACKING AXIS (RADIAL)

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20	ETA	4.0000		LON	475	83112	633	878	332	147	671	904	0.00	101101 101101	688	600	166	774	197	271	513	524	AXIS	ZETA*	43.416	43.081		42.659	•	•	40.273	•	37.077					27.253		
2	ö	RHG		UPSILON		0.83		0.54	0.42	0.30	0.18	0.08	0.0	j c	-0.16					•	٠	0.0	SECTION AXIS	UPSILÓN	90475	83988	7537	71134	1825	3663	2697	2000	9 6 6 6	29473	1001	3928	4183	09761	05636	01793
	£		ATA	THICKNESS	02343	04621	19087	3328	17236	1056	4603	7484	- 20	3.397	1904	1221	9912	28004	32	131		3008		UPS														0.0		
ROTOR	٠	I GN KK	INPUT DATA	THIC		0.0															Τ.	0	COORDINATES WITH ORIGIN AT	A. PHA	52169	22	38356	31449	. 24543	. 17636	10730	. 03823		80341			55477	47189	38901	30613
 	-7.03620	SECTI	MEANL I NE	ZETA*		•		•	37.819	•	•	26.778		16.845	13,463		•		•	6	42	-54.030	NATES H	•	-	7	-1			÷	-	- (;	, q	ģ	ģ	ò	9	· o	o O
STAGE	N	10	Σ	₹	69	126	727	3285	192	28	131	o 0	1 6	77	54	151	194			55	020	94		1/0	0.00811		•	0.02881	•	•	•	•	•				0.08988	0.09434	.0983	. 1017
	SYSTEM ORIGIN	ON NO		ALPHA	-1.5216	4	Ġ							0.06677					. 86	1.004	1.137	1.240	MEANLINE	r AL		0250	0200	0750	000	250	200	200		2600	000	3200	3500	3800	100	40
		SECTION		F		~	n	4	10 (10	~ (D C	,	2 =	<u>u</u>	13	4	50	16	7	©	0		PCT		Ö	o.	ö	o ·		o 0	o c	i c	Ö	Ö	Ö	Ö	ö	o.	_
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20	ETA 0.	4.0000	AXIS	ZETA*		9	19.260	17.592	15.919	14.207	10.00	. C.	6.402	3.651	0.157	-4.444	7	-19.423	-28.432	•	6	-53.608	ER	25	AXIS		UPSILON	0.904.75	0.90884	0.90619	0.85576	0.79858	0.74192	0.0000	0.00kg	0.000.00 0.000.00	0.000		0.43.64 0.38056	•	•
<u>0</u>	MU 0.	RHG	AT SECTION	UPSILON	.01779	.05082	.08114	.10876	. 13371	. 13603	7007	20673	-0.21776	-0.22513			- 21400 -	. 19144	. 15469	.09775		0.06524	CAMBER	97.025	AT SECTION	LOWER	ALPHA		•		-1.43777	•	-1.28631	•		•	٠	•	-0.02322 -0.74362		•
1. ROTOR	620 R O.	SECTION KK	TES WITH ORIGIN	ALPHA	w	•	•	٠.	0.10826	0.00	•	•		٠.			•	_•	0	1.10281	1.17188	1.24094	STAGGER	16.903	TES WITH ORIGIN	UPPER	UPSILON	ö	o	-	ö	o (00	o c	o c	o c	o c	0.3437	o c	0.2060	(1
STAGE	N Z -7.03620	0	NE COORDINATES	1/0		0.10703	0.10885	_	٠. ١	0.073			0.10488			0.09395		•	•	0.06250	•	•			ACE COORDINATES		ALPHA	-1.52169	-1,52522	.	-1.46748	•	-1.34268	•	•	•	•	-1.02254	•	7821	
	SYSTEM ORIGIN	SECTION NO	MEANL I NE	PCT AL	•	•	0.5300	•	•	0.6200	•	•	0.7400				•		œ.		. 97	1.0000	CHORD	2.8874	SURFACE		1/0	0.00811				•	0.02881	•	٠			•	0.06734	•	•
	COORD			T d	.	<u>o</u>	50	2	22	Š	A 6	3 0	200	28	58	30	9	32	33	34		36					F	-	N	ო	4	10 (1 Q	~ a	0 0	ָר פֿי		- 0	7 5		<u>r</u>

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OTOR	o.	¥	SURFACE COORDINATES WITH ORIGIN AT SECTION AXIS
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STAGE 1. ROTOR	03620	SECTION KK	NATES
STAGE	2 -7		COORD
	M ORIGIN	SECTION NO 10	SURFACE
	COORD SYSTEM ORIGIN Z -7.03620 R O.	SECT	

	UPSILON	0.29474	0.25541	0.21869	0.18429	0.15203	0.12176	•	0.06720	0.04273	0.01989	-0.00106	-0.02038	-0.03796	-0.05371	-0.06729	-0.07826	-0.08600	-0.08987	-0.08869	-0.08049	-0.06233	-0.02945	0.02378	O.06008	•	0.06524	0.69583	0.00698
LOWER	ALPHA	-0.57509	-0.49202	-0.40952	-0.32755	-0.24617	-0.16535	-0.08520	-0.00566	0.07342	0.15210	0.23038	0.30830	0.38591	0.46317	0.53954	0.61491	0.68881	0.76079	0.62950	0.89793	0.96992	1.04385	1.11189	1.14787	1.19394	1.24094	UPSILON	UPSILON
~	UPSILON	0.08381	0.02824	-0.02348	-0.07156	1617	5736	19516	22949	-0.26024	-0.28741	-0.31100	-0.33096	-0.34724	-0.35975	-0.36823	-0.37200	-0.36995	-0.36033	-0.33930	-0.30238	-0.24706		-0.07446	-0.03085	0.01014	0.06524	ALPHA -1.51222	_
UPPER	ALPHA	-0.70021	-0.61752	-0.53426	-0.45047	-0.36610	-0.28115	-0.19555	-0.10933	-0.02265	0.06443	•	•		0.41639	0.50577	0.59617	0.68803	0.78181	0.87885	0.97617	1.06994	1.16178	1.23186	1.25956	1.27011	1.24094	CENTER AT ALI	AT
	1/0	0.08494	0.08988	0.09434	0.09830	0.10175	0.10466	0.10703	0.10885	0.11008	0.11071	0.11073	0.11015	0.10898		0.10488	0.10194	0.09834	0.09395	0 08846	0.08148	0.07275	•		0.04505	•	•	RAD 0.01302	_
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	Œ			SURFACE ARC LENGTH	
TOR		¥		E ARC	ALPHA -0.02010 -0.02079 -0.02079
STAGE 1. ROTOR	α	SECTION KK	STAGGER 16.903	SURFAC	á
-	03620	SEC.	ις ·	•,	SECTION C.O. STREAMSURFACE SECTION C.O. BLADE AXIS STACKING AXIS (RADIAL)
STAGE	. 7 - 2				SECT!
	NIO	SECTION NO 10		15799	SECTION C.O. Streamsurface Section Blade axis Stacking axis (Radial)
	ORI	Z Z	CHGRD 2.8874	0.7	SECTION C.O. STREAMSURFAC BLADE AXIS STACKING AXI
	COORD SYSTEM ORIGIN Z -7.03620 R O.	SECTI	CHGRD 2.8874	AREA 0.715799	SECT STRE BLAD STAC
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PHASE I ROTOR

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i	2 E		UPSILON	. 7836	•				. 25591		.07934	•	. 04650		_ ,	15725	7.28	17123			•	•	SECTION AXIS		4	42	4	4	90	ਲ ∂	ਲ ਰ	ó	4 (š ē	ă	iò	ī	2 6	ić	N C	N
	œ)	0	0	0	0	o	0	0	0	0	o ·	P	Ģ (P	P	ė.	P	o ·	0	0	SECTI	UPSILON	78361	72453	66657	61027	55580	50335	45315		78805	90000	01494	17281	10011	23322	ָ מול	29	03084
£		ATA	THICKNESS	2960	05246	69960	3833	17664	21432	24984	27929	0220	32016	33163	3711	33664	3084	9	9889	30	N	8494	BIN AT	Š	o	•	٠	•	•		•	•	٠	•		•		<i>i</i> c			5
o .	7	INPUT DATA	THIC	•		•	٣.		•	•	•	•	Ö	<u>ب</u>	G			ი (N	Ö	Ġ	- 0	TH ORIGIN	ALPHA	49725	43216	36706	30197	3687	17178	.10668	0 to 0 to 0	¥/649	98030 80008	0107 N. 107	66403	0 to	58582	٥	ō ;	5157
	SECTION		ZETA*	258	611	723	137	213	866	216	930	844	270	720	515	051	267	696	623	Ø i	S	799	ES WITH	ALF	-1.45	4.7	-1.30	•	•	٠					o			Ü K	י סכ	-0.42	რ -
-7.03620	•/	MEANL I NE	12	42.	4.	38	37.	34.	30.	27.	23.	20.	17.	4	= '	eo (ej .		-18	-36	-53	-62.	COORDINATES		115	54	84	5	02	893	161	> 6	D) (2			2004	9234	5 6	- ! 0 {	737	49
N Z	11		¥	~	-	072	2171	97404	11325	981	835	29920	13256	091	19071	610	49611	266	519	90105	711	656		1/0	0	0	•	•	0.04005	•	•	•	•	•	•	•		0.097	- ·	-	Ξ
ØR I G I	NO.		ALPHA	-1.49	-1.42	-1.27072	Ξ.	0	-0.81	•	•		-0.13	•		•	•	•	•	•	•	•	MEANL I NE	AL		0250	0200	750	1000	220	200	2 6	000) () () ()	3500	2 (90	400
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20	ETA	3.5000	AXIS	ZETA*	20.012	ø.	ζ.	'n		•	<u>.</u> ,	•	٠	•		•		•	87 ·	17	7	Ŋ.	-65.591	E. 2	•	AXIS		S.		٠.	٠.							ò			•		
2	ö	R E E	SECTION A	ND	0125	6 00	127	07436	537	1431	3113	4575	01	755	7347	64	6852		11952		6 0 '	4	25	CAMBER 107.849	?	SECTION A	LOWER	ALPHA	49725	.48583	.47531	41567	.34443	. 27355	. 20311	. 13318	06387	. 99515	92698	.84591	76566	68619	
	£		¥	UPSILON	0.001	Ÿ	ö	٠	0.		 	5				- 0	Ξ.	•	ö		- (72	. 26			¥			Ť		<u>-</u>		-	_	-		7	o O	ġ.	0	0	P	
ROTOR	о	ION LL	WITH GRIGIN	ALPHA	.27346									. 42957	•	•	•	•	. 82014	•	.97637	•	•	STAGGER 11.328)	WITH ORIGIN	œ	UPSILON	•	•	0.76154	•	•	•	•	•	•	0.34051	•	•	•	•	
-	-7.03620	SECTION	COORDINATES				0				0										0			ST	•	COORDINATES	UPPER		49725	155	747	865	970	038	064	038	949	802	009	084	486	810	
STAGE	N	11		1/0	Ξ	٣.	- 2	Ξ.	Ξ.	Ξ.	0.12697	_	Ξ.	Ξ.	Ξ.	Ξ.	Ξ.	Ξ.	Ξ.	Ö	0.08803	٠.	٠.					ALPHA	-1.49	,-	,	_	-	_	-	_	.	-	<u>, </u>	o.	o.		
	SYSTEM ORIGIN	SECTION NO	MEANL I NE	PCT AL	•	٠	0.5300	•	0.5800	•	0.6500	•	٠	•	0.7700	•	0.8300	•	₩,	œ.	. 950	o,	8	CHORD 2.6556		SURFACE		1/0	.0111	.0111		.0185	•	•	0.04005	•	•	0.06007	•	•	.08	. 0864	
	COORD			ď	18	0	20	21	22	23	24	23	56	27	28	58	30	9	35		99	92	36					P	-	(Vi	n	4	SO.	9	7	Φ	O)	10		2	<u>.</u>	4	

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	ö	3.5000			UPSILON	.28185		. 2212	. 19402	٠	. 14491	.12286	. 10231	.08319	.06547	.04912	.03414	.02058	.00860	.00137		_		_	.00714	.03528	.08729	.17156	. 23001	. 26821	.26197	0.77246	0.17113
_	ETA	3.5	S		D	0	0	0	0	0	0	٥	0	0	0	0	0	0	0	o	9	0	o.	ö	0	0	0	Ö	0	0	0	O	0
20			AXIS																													Z	Z
2	o.	£	SECTION	LOWER	ALPHA	60740	-0.52921	45149	37417	-0.29739	22114	14530	62690	00536	08014	15453	22853	30203	37495	44638	51563	58142	64319	68188	75131	81301	88285	94882	98277	03872	0656	UPSILON	UPSILON
			SEC	ĭ	Y	0.6	9	4.	-0.3	23.		٠,		•	<u>0</u> .0	0.1	2.5	9.3	5.37	4.0	0.51	•	٠	0.6	•	•		9.0	96.0	7.03	7.	2	5
	3					T	Ŧ	0	7	ī	o	7	o	Ī	Ĭ	_	_	Ū			Ĭ	_		Ū	•	•	_		Ö	_	_	60	66
			Z		-	40	_			۰.	_	_			٠.	_		_	٠.		_		_		_		_					.48503	.06399
ROTOR		1	ORIGIN AT		UPSILGN	06406	01670	02746	06861	10692	14240	17503	20485	23191	25622	27774	29639	31208	32462	33374	33837	33674	32554	29826	24618	16665	05294	07652	3507	9572	26197	-	
2	0		¥1 TH		UPS		0.0	ö						-0.2		-0.2	-0.2	-0.3	-0.3	-0.3	-0.3	-0.3					0.0	9	<u>.</u> ٥	Ξ.	'4	⋖	< <
_:	6 2	SECTION	E K	UPPER				١	1	•	ī	•	•	ī	ī	ī	ī	ī	ī	ī	ī	ī	7	ī	ī	7	7	_				ILPH.	ALPHA
	362	S	ATE	2		7	N	Q	0	9	60	0)	7	on.	4	a	QI	(0	٨.	9	4	6 0	4	~	6	0	on.	٠.		10	9		AT /
STAGE	-7.03620		COORDINATES		ALPHA	7206	64262	56412	48520	40576	32578	24539	16467	08328	00214	02968	619	244 63	1279	41276	49974	59018	68464	78607	88838	98320	06989	13412	15761	16125	1065		
31	N		500		₹	-0.7	9.0								•	•	•	0.0	•	•	0.				٠	_•	<u>-</u>	- 1			-	CENT	CENTER
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	50	Š	รเ		1/0	09234	08260	10281	0737	1149	1514	1834	2106	2330	2504	2627	2697	2712	2672	2580	2433	2225	1928	1497	10857	09952	08803	07842	06964	06964	06964	.0	. 10
	STE	SECTION				0.	•		0	<u>.</u>	<u>.</u>	0	0	<u>.</u>	<u>.</u>	<u>.</u>	<u>.</u>	<u>.</u>	<u>.</u>	<u>.</u>	٦.	٣.	Ξ.	0				0	•	•	0.0		0
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50	ETA	3.5000	ER 49	6.29382	ze	· ~	N	
2	· o	SH HO	CAMBER 107.849	6.2	UPSILGN 0.02958	-0.0116	-0.0116	o.
~	£			SURFACE ARC LENGTH	ALPHA 0.00461	_	-0.00090	-0.00100
ROTOR	o o	SECTION LL	STAGGER 11.328	RFACE A		Ç	Ģ	9
-	3620	SECTI	STA	ns S		IN C. 0.		Ü
STAGE	2 -7.0					SECTIC		(RADIA
	COORD SYSTEM ORIGIN Z -7.03620 R O.	SECTION NO 11	CHØRD 2. 6556	AREA 0.738220	SECTION C.O.	STREAMSURFACE SECTION C. 0.	BLADE AXIS	STACKING AXIS (RADIAL)
	SYSTE	SECT	2 %	AREA	SEC.	STRE	BLAG	STA
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o	RHO		UPS	9.	0.6	'n	•	•	•	0.7	•					•	•	•	•		•	•	SECTION	UPSILON	68883	63988	59290	54767	50422	46249	42237	38377	34661	30384	26308	22436	18770	15310	202	Ξ	06181
₹	_	DATA	THICKNESS	04056	06247		_		. 21659	. 25138	. 28125	. 30646	32714	. 34321	. 35469	. 36092	. 36255	. 35890	34451	31140	26714	23980	ORIGIN AT	ă	-		ö			•	٠,•	•	•	•	•	•			٠	٠	
6	SECTION MM	INPUT	THI				0	0	0	0	0	0		0	0	0	0	0				-	WITH OR	ALPHA	.48244	1.42107	597	1.29834	1.23698	1.17561	1.11425	.05288	3.99152	3.91788	3.84424	09022	. 696	. 6233	. 5496	.4760	7
-7.03620	SEC	MEANL I NE	ZETA		•			•	•	25, 185			•					•	•	•	•	90	COORDINATES		10		•		•	1								٥- 8		•	t
N	12	_	¥ H	8244	40860	26224	1770	477	929	65177	1646	358	359	00730	447	106	1113	410	68634	79754	1721	2		1/0	0164	.0238	0.0311	•	•	•	•	•	•	0.07873	•	٠	Ÿ.	Ξ.	0.10966	٦.	_
SYSTEM ORIGIN	SECTION NO		ALPHA	-1.48	-1.40	-1.26	•	•	•	ö	•	•	•	•	•	•	•	•	•	•	0.89	O.	MEANL! NE	PCT AL		. 0250	.0500	.0750	. 1000	. 1250	.1500	. 1750	. 2000	. 2300	. 2600	. 2900	. 3200	. 3500	.3800	.4100	7400
	SEC		FT	-	N	၈	4	10	ဖ	^	€	G)	0	-	4	- -	4	<u></u>	16	17	18	<u>o</u>		PT P(0		0												ED.		
COGRD																					10	2		-										-	-	-			-		•

	· ·	3.0000		*	71	o	473	325	Ω !	25	N (740	2 2	388	248	363	8	195	161	8	83	27						UPSILON	. 68883	0.69749	•	. •	0.62359	•	•	٠	•	•	•	0.38826	٠	•
20	ETA	9.0	AXIS	ZETA*	18.987	17.6	6	'n.	14.0	'n.		, r	. K		-2.2	-9.3	-20.278	-35.15	-49.16		ö	-73.52		801	AXIS	•	•	_		_	_			•	•			•		•		
2	ö	RHO	SECTION	LON	.03547	108	01151	03250	05180	06923	08467	9000	796	0000	2356	11633	09744	05867	00926	692	120	870	4	112.801	SECTION		LOWER	ALPHA	. 48244	•	•	•	•	•	•	•	•		. 94647		79412	.7188
	₽		¥	UPSILO	0.03	0.0	ö	ó	0	0				· -		-0.1	-0.09	•	8	0.1	. 26	4.			A				-	7	•	-	•		•							o •
ROTOR	ö	ξ	H ORIGIN	¥	877	25513	18149	10785	03421	3943	11307	0/00/0	20004	40762	48126	55490	62854	70217	77581	94	082	2	C	75 56	H ORIGIN			UPSILON	•	•	•	•	•	•	•	•	•	•	. 27080	•	٠	•
<u>-</u> :	520 R	SECTION	FES WITH	ALPHA	-0.328	-0.25	-0.18	-0.10	0	ο,	- :		9.6	. 6	0.48	0.55	0.62			0.84	0.91	0.97	00410	3.356 5.356	TES WITH		UPPER												0			
STAGE	-7.03620	•,	COORDINATES	O	104	28.0	3184	3521	3821	4084	4306	0000	300	4707	4684	579	4336	3839	2969	698	614	72			COORDINATES			ALPHA	. 48244	.48727	.48083	.43915	.38276	. 32599	. 26881	.21127	. 15339	•	.03656			•
S)	N	7		7		Ξ.	Ξ.	٦.	•- '	~ '	0 0	- *			-	7	7	Ξ.	-	٣.	0.10	0							-	-	7	7	7	7	<u> </u>	-	7	-	-	o ·	o-	º
	SYSTEM ORIGIN	SECTION NO	MEANLINE	PCT AL	•		•	•	•	•	0.6500	•	•						0.9200	•			9	2.4654	SURFACE	; }		1/0	•	•		•	0.03114	•	•	•	•	•	0.07153	•	•	0.09214
	COORD S			Ā	18	9	50	2	22	53	22 0	0 0) (, a	9 0	90	31	35	33		98 0:							Fd	-	a	ო	4	IO.	9	~	Φ	O)	0	Ξ	7	<u>ლ</u>	4

20	ETA 0.	3.0000	AXIS		UPSILON	0.29681	. 2699	•	ú	٠	0.18002		_	٦.		0.10022					0.05791				٠.			C. 303\$6	9239679	0.45444	0.45870		ö	
2	₩.	RHO	SECTION	LOWER	ALPHA	-0.64416	-0.57007	-0.49656	-0.42360		•		•	•	•	0.07726	•	-	•	•	0.41521	•	0.52566	. 5672	. 6038	•	•	0.78716	0.82169	4	0.97218		5 UPSILON	
. ROTOR	o	SECTION MM	WITH ORIGIN AT	ER	UPSILON		0.03624	-0.00370		٦,	Ξ.	Ξ.	٣.	Ξ.	ú		-0.25773			-0.29804				Ċ	•	-0.09525	•	0.21844	0.30632	0.38552	.4587	ALPHA -1.4644	ALPHA 0.93415	
STAGE 1	Z -7.03620	12 SEC	E COORDINATES	UPPER	ALPHA	•	-0.67657	-0.60280	•	•		•	-0.22757	•	•	•	•	•	•	•	0.40003	•		•	0.80049	0.89680	•	•	1.05754	~	0.97218	¥	CENTER AT A	
	SYSTEM ORIGIN	SECTION NO	SURFACE		1/0	0.09834	0.10418	0.10966	Ξ	~	-	_	_	-	•	0.14084	0.14306		←.	٣.			7	Έ.	. 1383	٠.		0.10614	•	0.09727	•	Ö	RAD 0.12722	
	COORD				F.	<u>.</u>	16	17	18	9	50	21	22	23	24	22	5 6	27	58		၉ (35	33	34	35	36	37	38	99 9	64		표	

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20	ETÀ	3.0000	SER 80 î	6.15902	X 488
2	ö	£	CAMBER 112.803		UPSILGN 0.07034 0.00830 0.00830
ĸ	₹			SURFACE ARC LENGTH	ALPHA 0.02446 0.01723 0.01723
1. ROTOR	20 R 0.	SECTION MM	STAGGER 5.356	SURFACE	•
STAGE	2 -7.036	ร			SECTION (RADIAL)
	M ORIGIN ;	SECTION NO 12	CHORD 2.4654	0.774435	SECTION C.O. STREAMSURFACE SECTION C.O. BLADE AXIS STACKING AXIS (RADIAL)
	COORD SYSTEM ORIGIN Z -7.03620 R 0.	SECT	Į.	AREA	STR BPLA STA

	ö	<u>o</u>																																						
	ETA	2.5000																					G	ZETA*	448	.01	. 981				•		. 223		•	617	.521	286	930	ľ
20	_			UPSILON	61509	56814	48095	40103	32662	25060	17575	11093	01/0	7800	7000	6922	7505	05822	0223	13547	6771	5542	AXI	Ñ	33	33	9	<u></u>	8	5 (N	20 0	20	27	26	23	24	8	N (0 0	•
2	ö	R E		UPS	•	•	•	•) ;						•	•	•	0.0	SECTION AXIS	z	60	21	48	2	26	<u> </u>	/ N 0	32.5	63	61	81	37	4 50	0 1 0	777	-
	∑			κ																				UPSILON	0.61509		0.54048	•	0.47092	0.437	0.4052/ 0.3236K	0.34275	0.30663	0.27161	0.23781		<u>, </u>	4 :	0.117	D)
~			DATA	THICKNESS	05414	07433	11342	15016	18416	21858	25267	28304	91018	354-C	27007	38521	39426	39833	39013	35952	31680	29466	ORIGIN AT																	
ROTOR	ö	Z	INPUT	THIO		٠				0	•	0 0	•							•	•	0	H OR	¥	46853	41087	35322	29556	23790	927	12238	00727	93808	86889	79970	73051	66132	- (294 278	>
	Œ	NO I			_	_	•	•	_	/ 0	-						_			_	_	_	F I A	ALPHA	.46	•	•	•	٠		•	•		. 86		٠		ו יִּח	U 4 V K	7
.	-7.03620	SECTION	MEANL I NE	ZETA*		•	30.913			25.806		o (700.0	· -	- «		_	•	•	ın.		2.019	COORDINATES WITH		-	-	7	Ţ	Ţ,	-	7	ī	P	P	ó	P	o (o (P	,
STAGE	-7.0		MEA		n	(C)	n	CV.	W	(N)	<i>(</i> 0	.	- •		•		•	7	-3	-51	-63	-72	SRDIN	0	02347	03052	03751	139	05116	87750	05425	07666	08377)64	09727	366	0979	990	821	2
Ġ	7	က		_	က္	ဖွ	<u>თ</u>	=	Ç.	0	.	.	7	ŧ -	. 7	. <u>N</u>	10	က္	0	4	Ö	o		1/0	•	•	•	•	•						•	•	- - ,	- 1		-
	GRIGIN	P P		ALPHA	46853	. 39686	. 25499	11491	.97662	82619	. 66428	. 50488	3400g	2048	00800	23602	36615	48823	59750	69404	77730	83780	MEANL I NE		0	0	0	0	0 (5 (5 (0	0	0	0	0	0 (D (0 0	,
	8				-	7	7	7	P	o ·	o ·	o o	2 (ָרָ רְ	c	0	O	o	o	o	o	o	MEA	AL.		0220	0200	0720	000	000	200	000	2300	2600	2900	3200	3500	3800	0 0	1
	SYSTEM	SECTION		FT	-	~	က	4	EO.	9	~	6 0 (» (2 -	- 0	. E	4	13	16	17	9	<u>o</u>		PCT	o.				٠.,						-	-			o c	
	COORD																			1	06	;		PT		a	ო	4	K D (ום	~ a	a	5		12		4 1	0 (9 1	-

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50	ETA	2.5000	AXIS	ZETA*	•	•	•	4 (13.620		0	7.506	5.459	2.451	-2.114	•				-57.375			CAMBER	112.423	AXIS		בֿ	Ö	o	ö	o ·		o c			o c	i c	ic	ò	Ö	,
2	ö	RHO	SECTION	LON	068.80	04714	02.711	00840	(1096)	03911	05132	06153	05942	436	07474	06793	04923	00824	52700	19534	270	Ď	₹ S	112.	SECTION	LOWER	ALPHA	. 46853	•	٠	٠	•		•	•	. 00002	•	٠			•
	æ		AT	UPSILON	0.06	0.0	•		2.5		, i	ö	ö	o ·	· •	0	<i>.</i>		٠			9			A			-													
ROTOR	ö	NN NO	TH ORIGIN	ALPHA	38456	31537	24618	7696	8//01	03020	09978	16897	23816	30735	37654	44573	51492	56411	65530	72249	1000	00/5	GER	002	TH ORIGIN		UPSILON	•	•	•	0.54769		0.46127								
<u></u>	.03620 R	SECTIO	ATES WI	AL.	ö							•		•	•	•		٠	•	0.0	•	•	STAG	-1.002	ATES WI	UPPER		ဗ	0	so.	80 ·	o	20 0	D C	> <	1 (7	1 L	~ u	o co	•
STAGE	z -7.0		COORDINATES WITH	1/c	13183	13677	14149	14596	150018	15800	16146	16447	16707	16932	17117	17245	17252	1 7008	9820	14958	2016	4//2			COORDINATES WITH		ALPHA	-1.4685	•	•	-1.4300	•	-1.32198	•	•	11.1303	•	•	-0.91546		•
		13	MEANLINE	•	Ö	ö	.			Ö	ö	ö	Ö	0	ö	o (o e				<i>i</i> c				SURFACE															• •	_
	SYSTEM ORIGIN	SECTION NO	MEA	PCT AL		•	•	•	0.0800				•	•	•	•		•	•	0.9500	•	. 0000	CHORD	2.3067	S		1/0			•	•	0.03751	0.0443	0.03116	•		٠	•	0.08377	•	•
	COORD S	-		F		<u>o</u>	50	2	N 6	4	10 10 10	5 8	27	58	58	30	3	35	, ,	l d	. O	2					F	-	N	က	4	10	1 02	~ a	0 0	9 C		- 0	 4 G	5 4	ì

20	ETA 0.	2.5000	AXIS		UPSILON	0.31406		0.26862	0.24841	0.23004		=	Τ.	0.17125	Ξ.	ς.	-	_	~	•	0.12074	,-	٣.	Ξ.		0.17431	•		•	ĸ	0.65542	0.59828	
ê	M ∪ 0.	R D	SECTION	LOWER	ALPHA	-0.68071	-0.61078	-0.54152	-0.47297			-0.26996					٠.	0.12965		•	0.31570	•	•	0.44272	•	.4988	•	.6268	: 6631		0.83780		7 UPSILGN
KO LOK	.0	NN NOI.	WITH ORIGIN AT	œ	UPSILON	0.09668	.0583	•	-0.01288	-0.04542	-0.07575	-0.10393	-0.13007			-0.19879	•							•		٠	•	٠	0.48063	0.57721	4	PHA -1.44315	ALPHA 0.80547
9176	z -7.03620	13 SECTION	COORDINATES	UPPER	ALPHA	-0.78031	-0.71185	-0.64273	-0.57290		•	-0.36077		•			•		•	•	0.29899		•	•	•	0.80776	0.68172	•	.9570	0.94115	0.83780		AT
	COORD SYSTEM ORIGIN	SECTION NO 1	SURFACE		1/0	0.10366	0.10979	0.11566	0.12128	٣.	. 13	.13	-	Τ.	Ψ.	0.15420	٣.	Τ.	٣.	٣.	0.16932	٦.	٦.	٦.	٣.	0.16296	٦.	٣.	0.12774	7	0.12774	RAL C.03045	RAD 0.15355
	COORD				P		16	17	16	<u>.</u>	50	2	22	23	24	22	56	27			ဓ ၁8	31	35	33	34	33	36	37	38	30	4	ה ה	

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50	ETA	2.5000	3ER 123	6.09552	×	<u>0</u>	22	22	
9	o.	S.	CAMBER 112.423		UPSILON	0.12830	0.02822	0.02822	Ö
	D E			SURFACE ARC LENGTH	ALPHA	0.03806	0.03536	0.03536	-0.00100
GTOR	ö	Z	K 0	CE ARC	Y.	ö	ö	ö	ŏ. o-
-	8 2	SECTION	STAGGER -1.002	SURFA			0		
STAGE 1. ROTOR	-7.0362	SE					CTION		(ADIAL)
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	COORD SYSTEM GRIGIN Z -7.03620 R 0.	SECTION NO 13	RD 067	AREA 0.823718		SECTION C. G.	STREAMSURFACE SECTION C.O.	BLADE AXIS	STACKING AXIS- (RADIAL)
	SYSTEM	SECTION	CHGRD 2.3067	AREA		SECT	STRE	BLAD	STAC
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	ZETA1* ZETA2*	55.13		•	•	29.81	•	5.76	•		-53.61	•	-73.53	-78.67
50	ZETA1*	56.21	54.09	52.35	50.83	49.44	48.31	47.25	45.79	44.29	43.42	42.26	39.27	33.45
2	TM/C	0.02561	0.02618	0.03079	0.04044	0.05289	0.06380	0.07294	0.08267	0.09541	0.11073	0.12712	0.14707	0.17252
ROTOR	CAMBER	1.00			11.76	19.63	28.46	41.50	61.43	83.31	97.02	07.85		12.42
	STAGGER CAMBER	58.59	55.60	51.58	46.26	41.29	36.51	47	37	29	06	_	5.36 1	-1.00 1
STAGE 1.	CHORD	3.7610	3.9107	3.9279	3.8194	3.7298	3.6588	3.6019	3.4348	3.1597	2.8874	2.6556	2.4654	2.3067
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